

Group Meeting (MN2L)

10/05/2021

1. Time integration in PFEM

2. Results comparison:
Backward-Euler & α -Method

3. Explicit time integration scheme
used in PFEM-2

1. Time integration in PFEM

2. Results comparison:
Backward-Euler & α -Method

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Time Integration in PFEM

Motivation

- Understand the different time integration schemes.
- Study the influence of time integration methods in PFEM.

Some time integration schemes in dynamic problems

Linear momentum equation

$$\mathbf{M} \dot{\mathbf{v}} + \mathbf{K} \mathbf{v} - \mathbf{D}^T \mathbf{p} = \mathbf{f}^{\text{ext}}$$

PFEM Framework:

- Incompressible Newtonian Fluid
- PSPG stabilization
- Piccard Algorithm

Some time integration schemes in dynamic problems

Linear momentum equation

$$\mathbf{M} \dot{\mathbf{v}} + \mathbf{K} \mathbf{v} - \mathbf{D}^\top \mathbf{p} = \mathbf{f}^{\text{ext}}$$

Where : $\frac{d\mathbf{v}(\mathbf{x}^p)}{dt} = \dot{\mathbf{v}}(t, \mathbf{x}^p)$

integration : $\int d\mathbf{v} = \int \dot{\mathbf{v}}(t, \mathbf{x}^p) dt$

Time discret. : $\mathbf{v}_{n+1}(\mathbf{x}_{n+1}^p) - \mathbf{v}_n(\mathbf{x}_n^p) = \int_{t_n}^{t_{n+1}} \dot{\mathbf{v}}(\tau, \mathbf{x}_\tau^p) d\tau$

Time step : $\Delta t = t_{n+1} - t_n$

Some time integration schemes in dynamic problems

Linear momentum equation

$$\mathbf{M} \dot{\mathbf{v}} + \mathbf{K} \mathbf{v} - \mathbf{D}^T \mathbf{p} = \mathbf{f}^{\text{ext}}$$

Where : $\frac{d\mathbf{x}^p}{dt} = \mathbf{v}(t, \mathbf{x}^p)$

integration : $\int d\mathbf{x} = \int \mathbf{v}(t, \mathbf{x}^p) dt$

Time discret. : $\mathbf{x}_{n+1}^p - \mathbf{x}_n^p = \int_{t_n}^{t_{n+1}} \mathbf{v}(\tau, \mathbf{x}_\tau^p) d\tau$

Time step : $\Delta t = t_{n+1} - t_n$

Some time integration schemes in dynamic problems

Exact expression for integrating state variables:

$$\mathbf{v}_{n+1}(\mathbf{x}_{n+1}^p) = \mathbf{v}_n(\mathbf{x}_n^p) + \int_{t_n}^{t_{n+1}} \dot{\mathbf{v}}(\tau, \mathbf{x}_\tau^p) d\tau$$
$$\mathbf{x}_{n+1}^p = \mathbf{x}_n^p + \int_{t_n}^{t_{n+1}} \mathbf{v}(\tau, \mathbf{x}_\tau^p) d\tau$$

$\dot{\mathbf{v}}(\tau, \mathbf{x}_\tau^p)$ and $\mathbf{v}(\tau, \mathbf{x}_\tau^p)$ are unknown time- and space-dependent functions.

$\dot{\mathbf{v}}(\tau, \mathbf{x}_\tau^p)$ and $\mathbf{v}(\tau, \mathbf{x}_\tau^p)$ need to be approximated. (Accuracy will depend on the accuracy of the approximation function, on the time and space discretization).

1) Assume $\dot{\mathbf{v}}(\tau, \mathbf{x}_\tau^p)$ constant between $[t_n, t_{n+1}]$ and around \mathbf{x}^p

1.a) Assume $\dot{\mathbf{v}}(\tau, \mathbf{x}_\tau^p) = \dot{\mathbf{v}}(t_n, \mathbf{x}_n^p) = \dot{\mathbf{v}}_n$ *(Explicit)*

Integrating the acceleration:

$$\mathbf{v}_{n+1}(\mathbf{x}_{n+1}^p) = \mathbf{v}_n(\mathbf{x}_n^p) + \int_{t_n}^{t_{n+1}} \dot{\mathbf{v}}_n d\tau$$

$$\mathbf{v}_{n+1}(\mathbf{x}_{n+1}^p) = \mathbf{v}_n(\mathbf{x}_n^p) + \Delta t \dot{\mathbf{v}}_n$$

(Forward Euler / Runge-Kutta)

Integrating the velocity function:

$$\mathbf{x}_{n+1}^p = \mathbf{x}_n^p + \int_{t_n}^{t_{n+1}} \mathbf{v}(\tau, \mathbf{x}_\tau^p) d\tau$$

$$\mathbf{x}_{n+1}^p = \mathbf{x}_n^p + \int_{t_n}^{t_{n+1}} \mathbf{v}_n(\mathbf{x}_n^p) + (\tau - t_n) \dot{\mathbf{v}}_n(\mathbf{x}_n^p) d\tau$$

$$\mathbf{x}_{n+1}^p = \mathbf{x}_n^p + \Delta t \mathbf{v}_n(\mathbf{x}_n^p) + \frac{\Delta t^2}{2} \dot{\mathbf{v}}_n(\mathbf{x}_n^p)$$

1) Assume $\dot{\mathbf{v}}(\tau, \mathbf{x}_\tau^p)$ constant between $[t_n, t_{n+1}]$ and around \mathbf{x}^p

1.b) Assume $\dot{\mathbf{v}}(\tau, \mathbf{x}_\tau^p) = \dot{\mathbf{v}}(t_{n+1}, \mathbf{x}_{n+1}^p) = \dot{\mathbf{v}}_{n+1}$ *(Implicit)*

Integrating the acceleration:

$$\mathbf{v}_{n+1}(\mathbf{x}_{n+1}^p) = \mathbf{v}_n(\mathbf{x}_n^p) + \int_{t_n}^{t_{n+1}} \dot{\mathbf{v}}_{n+1} d\tau$$

$$\mathbf{v}_{n+1}(\mathbf{x}_{n+1}^p) = \mathbf{v}_n(\mathbf{x}_n^p) + \Delta t \dot{\mathbf{v}}_{n+1} \quad \text{(Backward Euler)}$$

Integrating the velocity function:

$$\mathbf{x}_{n+1}^p = \mathbf{x}_n^p + \int_{t_n}^{t_{n+1}} \mathbf{v}(\tau, \mathbf{x}_\tau^p) d\tau$$

$$\mathbf{x}_{n+1}^p = \mathbf{x}_n^p + \int_{t_n}^{t_{n+1}} \mathbf{v}_n(\mathbf{x}_n^p) + (\tau - t_n) \dot{\mathbf{v}}_{n+1}(\mathbf{x}_{n+1}^p) d\tau$$

$$\mathbf{x}_{n+1}^p = \mathbf{x}_n^p + \Delta t \mathbf{v}_n(\mathbf{x}_n^p) + \frac{\Delta t^2}{2} \dot{\mathbf{v}}_{n+1}(\mathbf{x}_{n+1}^p)$$

1) Assume $\dot{\mathbf{v}}(\tau, \mathbf{x}_\tau^p)$ constant between $[t_n, t_{n+1}]$ and around \mathbf{x}^p

1.c) Assume $\dot{\mathbf{v}}(\tau, \mathbf{x}_\tau^p) = \dot{\mathbf{v}}(t_{n+1}, \mathbf{x}_{n+1}^p) = \dot{\mathbf{v}}_{n+1}$ *(Implicit)*
 $\mathbf{v}(\tau, \mathbf{x}_\tau^p) = \mathbf{v}(t_{n+1}, \mathbf{x}_{n+1}^p) = \mathbf{v}_{n+1}$

Integrating the acceleration:

$$\mathbf{v}_{n+1}(\mathbf{x}_{n+1}^p) = \mathbf{v}_n(\mathbf{x}_n^p) + \int_{t_n}^{t_{n+1}} \dot{\mathbf{v}}_{n+1} d\tau$$

$$\mathbf{v}_{n+1}(\mathbf{x}_{n+1}^p) = \mathbf{v}_n(\mathbf{x}_n^p) + \Delta t \dot{\mathbf{v}}_{n+1}$$

(Backward Euler)

Integrating the velocity function:

$$\mathbf{x}_{n+1}^p = \mathbf{x}_n^p + \int_{t_n}^{t_{n+1}} \mathbf{v}(\tau, \mathbf{x}_\tau^p) d\tau$$

$$\mathbf{x}_{n+1}^p = \mathbf{x}_n^p + \int_{t_n}^{t_{n+1}} \mathbf{v}_{n+1}(\mathbf{x}_{n+1}^p) d\tau$$

$$\mathbf{x}_{n+1}^p = \mathbf{x}_n^p + \Delta t \mathbf{v}_{n+1}(\mathbf{x}_n^p)$$

(Backward Euler)

1) Assume $\dot{\mathbf{v}}(\tau, \mathbf{x}_\tau^p)$ constant between $[t_n, t_{n+1}]$ and around \mathbf{x}^p

1.a) Assume $\dot{\mathbf{v}}(\tau, \mathbf{x}_\tau^p) = \dot{\mathbf{v}}(t_n, \mathbf{x}_n^p) = \dot{\mathbf{v}}_n$ *(Explicit)*

$$\mathbf{v}_{n+1}(\mathbf{x}_{n+1}^p) = \mathbf{v}_n(\mathbf{x}_n^p) + \Delta t \dot{\mathbf{v}}_n$$

$$\mathbf{x}_{n+1}^p = \mathbf{x}_n^p + \Delta t \mathbf{v}_n(\mathbf{x}_n^p) + \frac{\Delta t^2}{2} \dot{\mathbf{v}}_n(\mathbf{x}_n^p)$$

1.b) Assume $\dot{\mathbf{v}}(\tau, \mathbf{x}_\tau^p) = \dot{\mathbf{v}}(t_{n+1}, \mathbf{x}_{n+1}^p) = \dot{\mathbf{v}}_{n+1}$ *(Implicit)*

$$\mathbf{v}_{n+1}(\mathbf{x}_{n+1}^p) = \mathbf{v}_n(\mathbf{x}_n^p) + \Delta t \dot{\mathbf{v}}_{n+1}$$

$$\mathbf{x}_{n+1}^p = \mathbf{x}_n^p + \Delta t \mathbf{v}_n(\mathbf{x}_n^p) + \frac{\Delta t^2}{2} \dot{\mathbf{v}}_{n+1}(\mathbf{x}_{n+1}^p)$$

1.c) Assume $\dot{\mathbf{v}}(\tau, \mathbf{x}_\tau^p) = \dot{\mathbf{v}}(t_{n+1}, \mathbf{x}_{n+1}^p) = \dot{\mathbf{v}}_{n+1}$

$$\mathbf{v}(\tau, \mathbf{x}_\tau^p) = \mathbf{v}(t_{n+1}, \mathbf{x}_{n+1}^p) = \mathbf{v}_{n+1}$$

(Implicit)

$$\mathbf{v}_{n+1}(\mathbf{x}_{n+1}^p) = \mathbf{v}_n(\mathbf{x}_n^p) + \Delta t \dot{\mathbf{v}}_{n+1}$$

$$\mathbf{x}_{n+1}^p = \mathbf{x}_n^p + \Delta t \mathbf{v}_{n+1}(\mathbf{x}_n^p)$$

1) Assume $\dot{\mathbf{v}}(\tau, \mathbf{x}_\tau^p)$ constant between $[t_n, t_{n+1}]$ and around \mathbf{x}^p

1.d) Assume $\dot{\mathbf{v}}(\tau, \mathbf{x}_\tau^p) = (1 - \gamma)\dot{\mathbf{v}}_n + \gamma \dot{\mathbf{v}}_{n+1}$ *(Generalized mid-point rule)**
*($\gamma = 1/2$, trapezoidal rule)**
*($\gamma = 0$, Forward Euler)**
*($\gamma = 1$, Backward Euler)**

Integrating the acceleration:

$$\mathbf{v}_{n+1}(\mathbf{x}_{n+1}^p) = \mathbf{v}_n + (1 - \gamma) \Delta t \dot{\mathbf{v}}_n + \gamma \Delta t \dot{\mathbf{v}}_{n+1}$$

Integrating the velocity function:

$$\mathbf{x}_{n+1}^p = \mathbf{x}_n^p + \Delta t \mathbf{v}_n + (1 - \gamma) \frac{\Delta t^2}{2} \dot{\mathbf{v}}_n + \gamma \frac{\Delta t^2}{2} \dot{\mathbf{v}}_{n+1}$$

* Lovrić, A., Dettmer, W. G., Kadapa, C., & Perić, D. (2018). A new family of projection schemes for the incompressible Navier–Stokes equations with control of high-frequency damping. *CMAME*, 339, 160-183.

1) Assume $\dot{\mathbf{v}}(\tau, \mathbf{x}_\tau^p)$ constant between $[t_n, t_{n+1}]$ and around \mathbf{x}^p

1.e) Assume $\dot{\mathbf{v}}(\tau, \mathbf{x}_\tau^p) = (1 - \gamma)\dot{\mathbf{v}}_n + \gamma \dot{\mathbf{v}}_{n+1}$ (for velocities)

(Newmark)

$\dot{\mathbf{v}}(\tau, \mathbf{x}_\tau^p) = (1 - 2\beta)\dot{\mathbf{v}}_n + 2\beta \dot{\mathbf{v}}_{n+1}$ (for displacements)

Integrating the acceleration:

$$\mathbf{v}_{n+1}(\mathbf{x}_{n+1}^p) = \mathbf{v}_n + (1 - \gamma) \Delta t \dot{\mathbf{v}}_n + \gamma \Delta t \dot{\mathbf{v}}_{n+1}$$

Integrating twice the blue acceleration function:

$$\mathbf{x}_{n+1}^p = \mathbf{x}_n^p + \Delta t \mathbf{v}_n + (1 - 2\beta) \frac{\Delta t^2}{2} \dot{\mathbf{v}}_n + 2\beta \frac{\Delta t^2}{2} \dot{\mathbf{v}}_{n+1}$$

1) Assume $\dot{\mathbf{v}}(\tau, \mathbf{x}_\tau^p)$ constant between $[t_n, t_{n+1}]$ and around \mathbf{x}^p

1.f) Assume $\dot{\mathbf{v}}(\tau, \mathbf{x}_\tau^p) = (1 - \gamma)\dot{\mathbf{v}}_n + \gamma \dot{\mathbf{v}}_{n+1}$ (for velocities) (Newmark)

$\dot{\mathbf{v}}(\tau, \mathbf{x}_\tau^p) = (1 - 2\beta)\dot{\mathbf{v}}_n + 2\beta \dot{\mathbf{v}}_{n+1}$ (for displacements)

Weighted or Interpolated state variables:

$$\dot{\mathbf{v}}_{n+\alpha_m} = (1 - \alpha_m)\dot{\mathbf{v}}_n + \alpha_m \dot{\mathbf{v}}_{n+1}$$

$$\mathbf{v}_{n+\alpha_f} = (1 - \alpha_f)\mathbf{v}_n + \alpha_f \mathbf{v}_{n+1}$$

(Generalized α -Method)*

ρ_∞ : Spectral radius

To be used in:

$$\mathbf{M} \dot{\mathbf{v}}_{n+\alpha_m} + \mathbf{K} \mathbf{v}_{n+\alpha_f} - \mathbf{D}^\top \mathbf{p} = \mathbf{f}^{\text{ext}}$$

* Lovrić, A., Dettmer, W. G., Kadapa, C., & Perić, D. (2018). A new family of projection schemes for the incompressible Navier–Stokes equations with control of high-frequency damping. *CMAME*, 339, 160-183.

Time Integration : Generalized α -Method in PFEM

PFEM Framework:

- Incompressible Newtonian Fluid
- Velocity-Pressure formulation
- PSPG stabilization
- Piccard Algorithm

- Newmark Integration:

$$\mathbf{v}_{n+1}(\mathbf{x}_{n+1}^p) = \mathbf{v}_n + (1 - \gamma) \Delta t \dot{\mathbf{v}}_n + \gamma \Delta t \dot{\mathbf{v}}_{n+1} \quad (1)$$

$$\mathbf{x}_{n+1}^p = \mathbf{x}_n^p + \Delta t \mathbf{v}_n + (1 - 2\beta) \frac{\Delta t^2}{2} \dot{\mathbf{v}}_n + 2\beta \frac{\Delta t^2}{2} \dot{\mathbf{v}}_{n+1} \quad (2)$$

- α -Method:
$$\dot{\mathbf{v}}_{n+\alpha_m} = (1 - \alpha_m) \dot{\mathbf{v}}_n + \alpha_m \dot{\mathbf{v}}_{n+1} \quad (3)$$

$$\mathbf{v}_{n+\alpha_f} = (1 - \alpha_f) \mathbf{v}_n + \alpha_f \mathbf{v}_{n+1} \quad (4)$$

Time Integration : Generalized α -Method in PFEM

Working (1) :
$$\dot{\mathbf{v}}_{n+1} = \frac{1}{\gamma \Delta t} (\mathbf{v}_{n+1} - \mathbf{v}_n) - (1/\gamma - 1) \dot{\mathbf{v}}_n \quad (5)$$

(5) in (3) :
$$\dot{\mathbf{v}}_{n+\alpha_m} = \frac{\alpha_m}{\gamma \Delta t} (\mathbf{v}_{n+1} - \mathbf{v}_n) + (1 - \alpha_m/\gamma) \dot{\mathbf{v}}_n \quad (6)$$

(4) and (6) in :
$$\mathbf{M} \dot{\mathbf{v}}_{n+\alpha_m} + \mathbf{K} \mathbf{v}_{n+\alpha_f} - \mathbf{D}^T \mathbf{p} = \mathbf{f}^{\text{ext}}$$

... yields :
$$\mathbf{M} \frac{\alpha_m}{\gamma \Delta t} \mathbf{v}_{n+1} + \mathbf{K} \alpha_f \mathbf{v}_{n+1} - \mathbf{D}^T \mathbf{p}_{n+1} = \quad (7)$$

$$\mathbf{f}^{\text{ext}} + \mathbf{M} \left(\frac{\alpha_m}{\gamma \Delta t} \mathbf{v}_n - (1 - \alpha_m/\gamma) \dot{\mathbf{v}}_n \right) + \mathbf{K} (\alpha_f - 1) \mathbf{v}_n$$

(In blue the added terms w.r.t. Backward Euler integration scheme)

Time Integration : Generalized α -Method in PFEM

PFEM Framework:

- Incompressible Newtonian Fluid
- **Position-Pressure formulation**
- PSPG stabilization
- Piccard Algorithm

- Newmark Integration:

$$\mathbf{v}_{n+1}(\mathbf{x}_{n+1}^p) = \mathbf{v}_n + (1 - \gamma) \Delta t \dot{\mathbf{v}}_n + \gamma \Delta t \dot{\mathbf{v}}_{n+1} \quad (1)$$

$$\mathbf{x}_{n+1}^p = \mathbf{x}_n^p + \Delta t \mathbf{v}_n + (1 - 2\beta) \frac{\Delta t^2}{2} \dot{\mathbf{v}}_n + 2\beta \frac{\Delta t^2}{2} \dot{\mathbf{v}}_{n+1} \quad (2)$$

- α -Method:
$$\dot{\mathbf{v}}_{n+\alpha_m} = (1 - \alpha_m) \dot{\mathbf{v}}_n + \alpha_m \dot{\mathbf{v}}_{n+1} \quad (3)$$

$$\mathbf{v}_{n+\alpha_f} = (1 - \alpha_f) \mathbf{v}_n + \alpha_f \mathbf{v}_{n+1} \quad (4)$$

Time Integration : Generalized α -Method in PFEM

$$\text{from (2) : } \dot{\mathbf{v}}_{n+1} = \frac{1}{\beta \Delta t^2} (\mathbf{x}_{n+1} - \mathbf{x}_n) - \frac{1}{\beta \Delta t} \mathbf{v}_n + \left(1 - \frac{1}{2\beta}\right) \dot{\mathbf{v}}_n \quad (5)$$

$$(5) \text{ in (1) : } \mathbf{v}_{n+1} = \frac{\gamma}{\beta \Delta t} (\mathbf{x}_{n+1} - \mathbf{x}_n) + \frac{\beta - \gamma}{\beta} \mathbf{v}_n + \left(\frac{2\beta - \gamma}{2\beta}\right) \Delta t \dot{\mathbf{v}}_n \quad (6)$$

$$(5) \text{ in (3) : } \dot{\mathbf{v}}_{n+\alpha_m} = \frac{\alpha_m}{\beta \Delta t^2} (\mathbf{x}_{n+1} - \mathbf{x}_n) - \frac{\alpha_m}{\beta \Delta t} \mathbf{v}_n + \left(1 - \frac{\alpha_m}{2\beta}\right) \dot{\mathbf{v}}_n \quad (7)$$

(6) in (4) :

$$\mathbf{v}_{n+\alpha_f} = \frac{\alpha_f \gamma}{\beta \Delta t} (\mathbf{x}_{n+1} - \mathbf{x}_n) + \left(1 - \frac{\alpha_f \gamma}{\beta}\right) \mathbf{v}_n + \alpha_f \Delta t \left(1 - \frac{\gamma}{2\beta}\right) \dot{\mathbf{v}}_n \quad (8)$$

Time Integration : Generalized α -Method in PFEM

... yields :

$$\mathbf{M} \frac{\alpha_m}{\beta \Delta t^2} (\mathbf{x}_{n+1} - \mathbf{x}_n) + \mathbf{K} \frac{\alpha_f \gamma}{\beta \Delta t} (\mathbf{x}_{n+1} - \mathbf{x}_n) - \mathbf{D}^\top \mathbf{p}_{n+1} = \quad (9)$$

$$\mathbf{f}^{\text{ext}} + \mathbf{M} \left(\frac{\alpha_m}{\beta \Delta t} \mathbf{v}_n - \left(1 - \frac{\alpha_m}{2\beta} \right) \dot{\mathbf{v}}_n \right) + \mathbf{K} \left(\left(\frac{\gamma \alpha_f}{\beta} - 1 \right) \mathbf{v}_n - \alpha_f \Delta t \left(1 - \frac{\gamma}{2\beta} \right) \dot{\mathbf{v}}_n \right)$$

(In blue the added terms w.r.t. Backward Euler integration scheme)

(In red the added terms w.r.t. α -Method integration scheme in a velocity-pressure formulation)

Time Integration : Generalized α -Method in PFEM

Summary

Backward-Euler & Velocity-Pressure

$$\mathbf{M} \frac{1}{\Delta t} \mathbf{v}_{n+1} + \mathbf{K} \mathbf{v}_{n+1} - \mathbf{D}^T \mathbf{p}_{n+1} = \mathbf{f}^{\text{ext}} + \mathbf{M} \frac{1}{\Delta t} \mathbf{v}_n$$

α -Method & Velocity-Pressure

$$\mathbf{M} \frac{\alpha_m}{\gamma \Delta t} \mathbf{v}_{n+1} + \mathbf{K} \alpha_f \mathbf{v}_{n+1} - \mathbf{D}^T \mathbf{p}_{n+1} = \\ \mathbf{f}^{\text{ext}} + \mathbf{M} \left(\frac{\alpha_m}{\gamma \Delta t} \mathbf{v}_n - (1 - \alpha_m/\gamma) \dot{\mathbf{v}}_n \right) + \mathbf{K} (\alpha_f - 1) \mathbf{v}_n$$

α -Method & Displacement-Pressure

$$\mathbf{M} \frac{\alpha_m}{\beta \Delta t^2} (\mathbf{x}_{n+1} - \mathbf{x}_n) + \mathbf{K} \frac{\alpha_f \gamma}{\beta \Delta t} (\mathbf{x}_{n+1} - \mathbf{x}_n) - \mathbf{D}^T \mathbf{p}_{n+1} = \\ \mathbf{f}^{\text{ext}} + \mathbf{M} \left(\frac{\alpha_m}{\beta \Delta t} \mathbf{v}_n - \left(1 - \frac{\alpha_m}{2\beta} \right) \dot{\mathbf{v}}_n \right) + \mathbf{K} \left(\left(\frac{\gamma \alpha_f}{\beta} - 1 \right) \mathbf{v}_n - \alpha_f \Delta t \left(1 - \frac{\gamma}{2\beta} \right) \dot{\mathbf{v}}_n \right)$$

Nonlinear algorithm for Velocity-Pressure formulation

Backward-Euler

Known: $\mathbf{x}_n, \mathbf{v}_n, \dot{\mathbf{v}}_n$

1) Set $k = 0$

2) Initial guess: $\mathbf{x}_k = \mathbf{x}_n$

3) *While* (convergence is not reached)

3.1) Compute:

$$\mathbf{A}_{BE}(\mathbf{x}_k, \mathbf{v}_k)$$

$$\mathbf{b}_{BE}(\mathbf{x}_k, \mathbf{v}_n, \mathbf{v}_k)$$

3.2) Solve : $\mathbf{A}_{BE} \mathbf{q}_{n+1} = \mathbf{b}_{BE}$

3.3) Update : $\mathbf{x}_k = \mathbf{x}_n + \Delta t \mathbf{v}_{k+1}$

3.4) Set : $k = k + 1$

4) Set : $\mathbf{q}_{n+1} = \mathbf{q}_k$

Update : $\mathbf{x}_{n+1} = \mathbf{x}_n + \Delta t \mathbf{v}_{n+1}$

5) **RE-MESH (if necessary)**

α -Method

Known: $\mathbf{x}_n, \mathbf{v}_n, \dot{\mathbf{v}}_n$

1) Set $k = 0$

2) Initial guess: $\mathbf{x}_k = \mathbf{x}_n$

3) *While* (convergence is not reached)

3.1) Compute:

$$\mathbf{A}_{AM}(\mathbf{x}_k, \mathbf{v}_k, \gamma, \beta, \alpha_m, \alpha_f)$$

$$\mathbf{b}_{AM}(\mathbf{x}_k, \mathbf{v}_k, \mathbf{v}_n, \dot{\mathbf{v}}_n, \gamma, \beta, \alpha_m, \alpha_f)$$

3.2) Solve : $\mathbf{A}_{AM} \mathbf{q}_{n+1} = \mathbf{b}_{AM}$

3.3) Update : \mathbf{x}_k **using Newmark**

3.4) Set : $k = k + 1$

4) Set : $\mathbf{q}_{n+1} = \mathbf{q}_k$

Update : \mathbf{x}_{n+1} **using Newmark**

5) **RE-MESH (if necessary)**

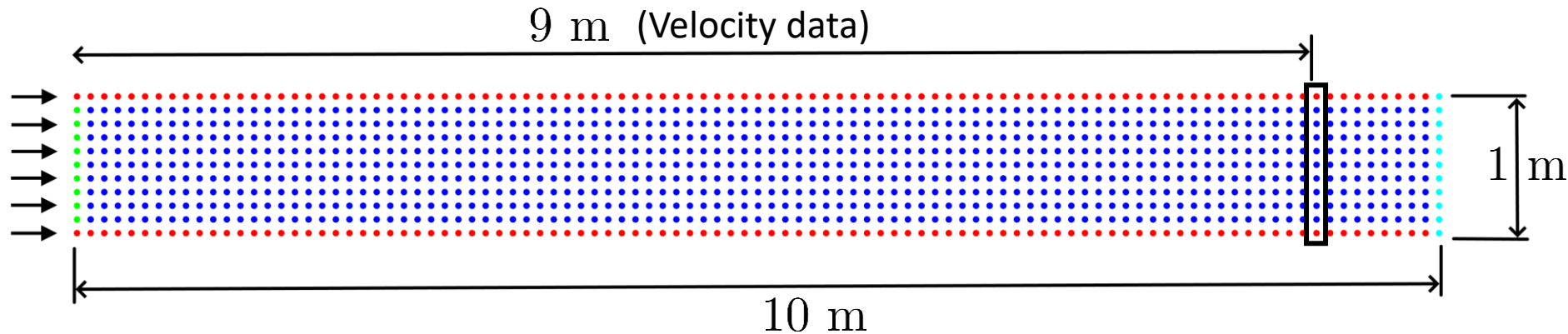
1. Time integration in PFEM

**2. Results comparison:
Backward-Euler & α -Method**

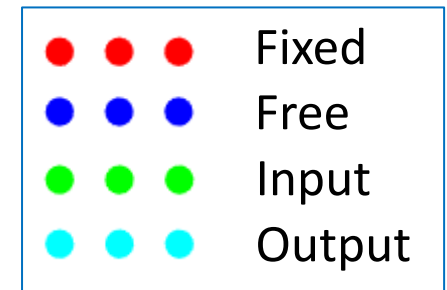
3. Explicit time integration scheme
used in PFEM-2

Comparison of time integration schemes

Test case : Flow between 2 plates.

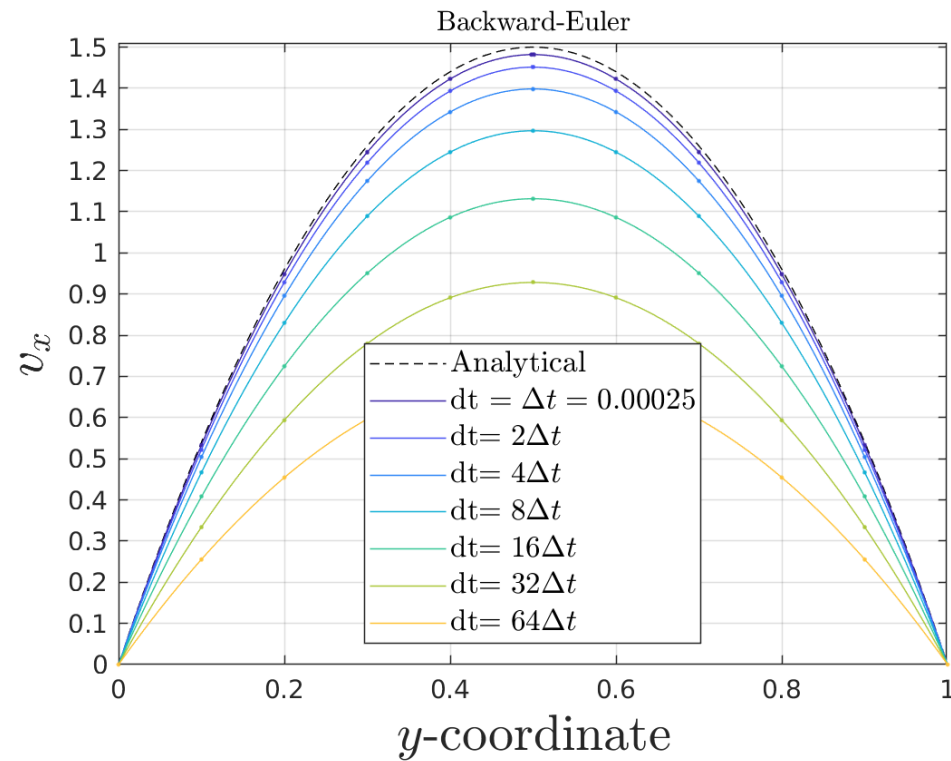


Num. Initial Particles	: 1138
Input velocity	: 1 m/s
Density	: 1000 kg/m^3
Dynamic viscosity	: 50 Pa s.
Simulation span	: 5 seconds
Initial time step	: 0.0001
Maximum time step	: 0.00025 , 0.0005, 0.001, 0.002, 0.004, 0.008, 0.016
(7 cases)	: [Δt , $2\Delta t$, $4\Delta t$, $8\Delta t$, $16\Delta t$, $32\Delta t$, $64\Delta t$]

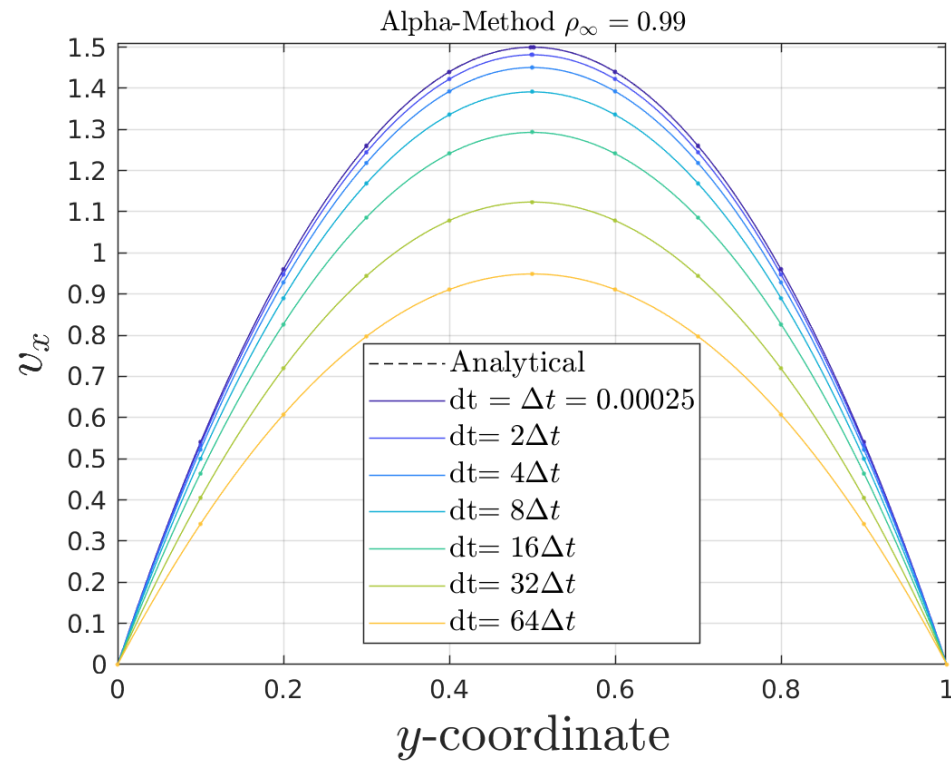


Flow Between 2 plates : Results (BE and α M)

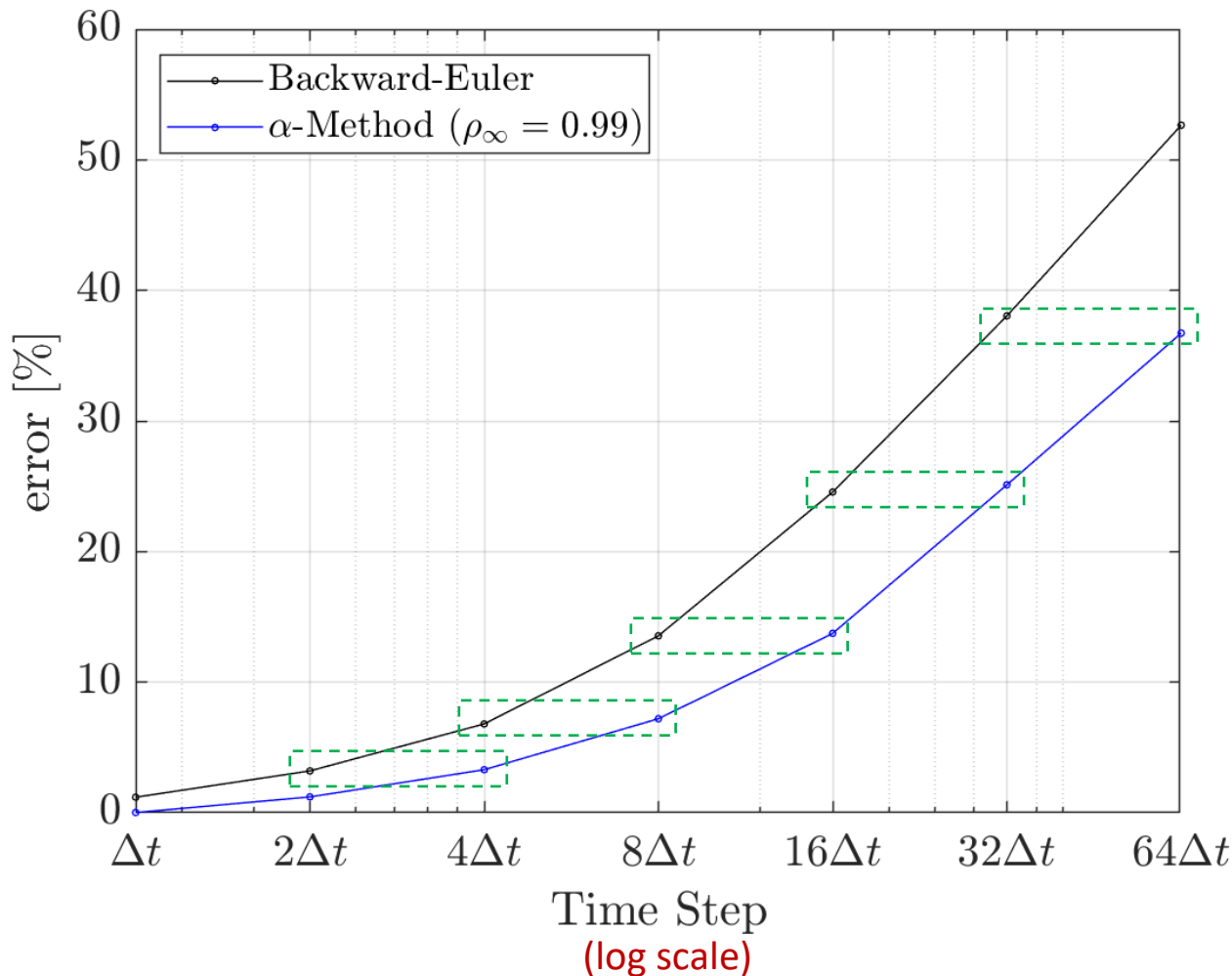
Backward-Euler



α -Method



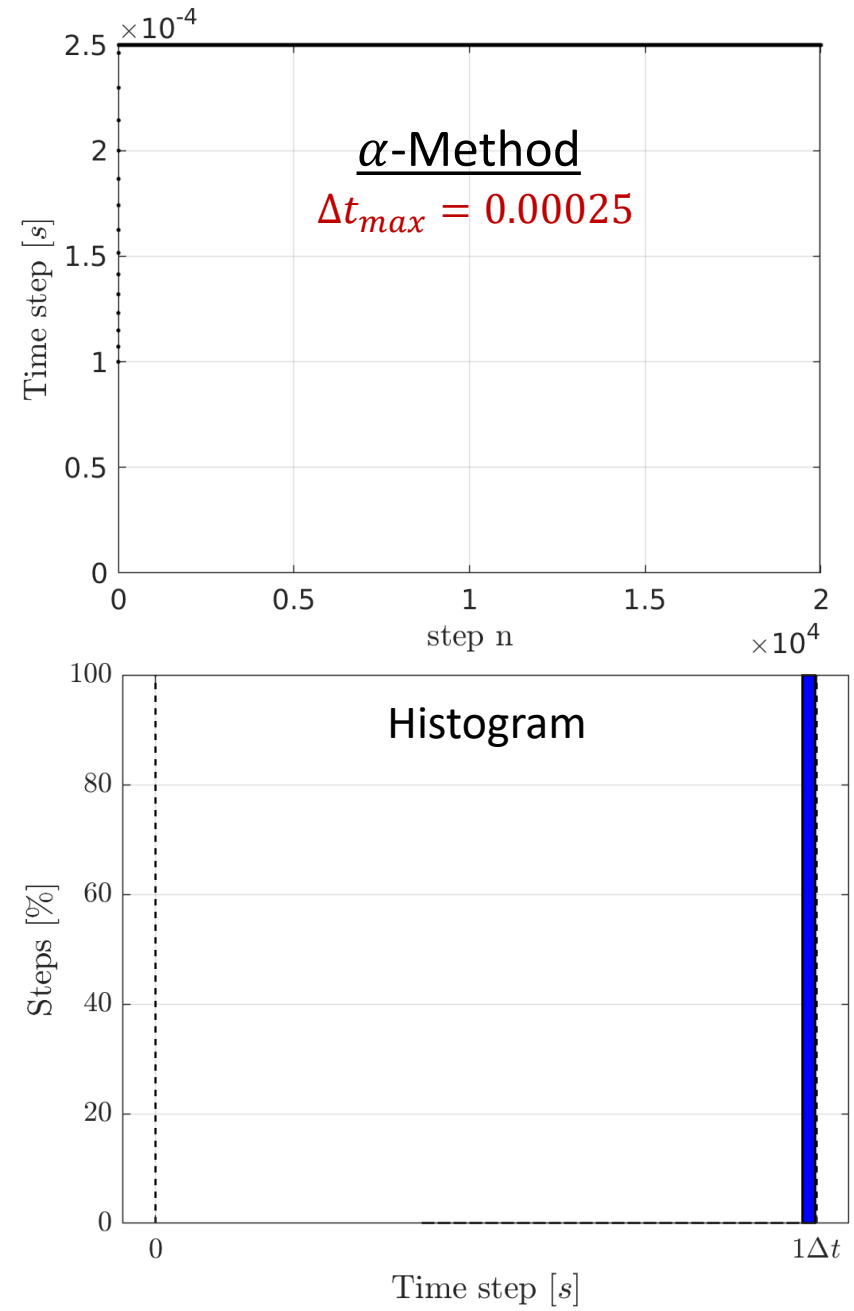
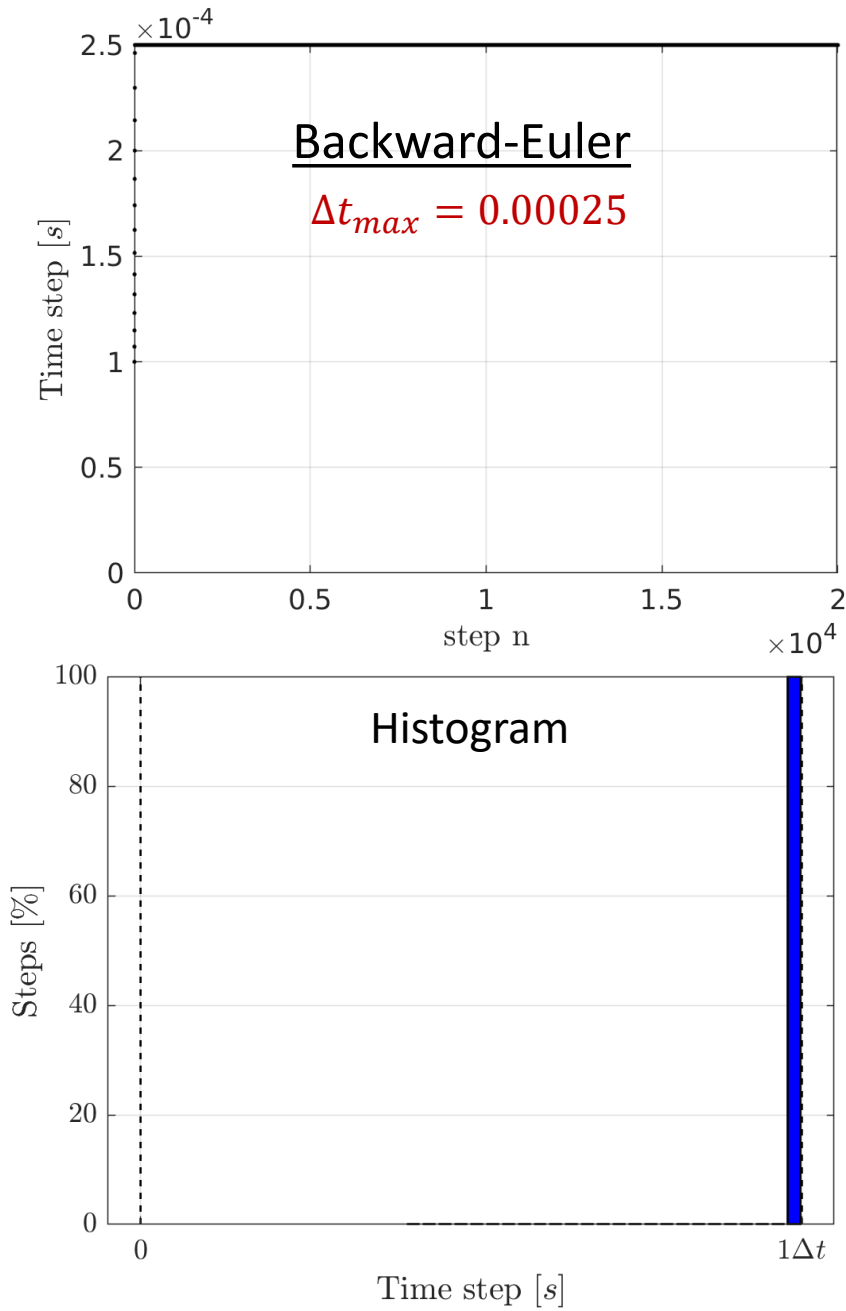
Flow Between 2 plates : Results (BE and α M)



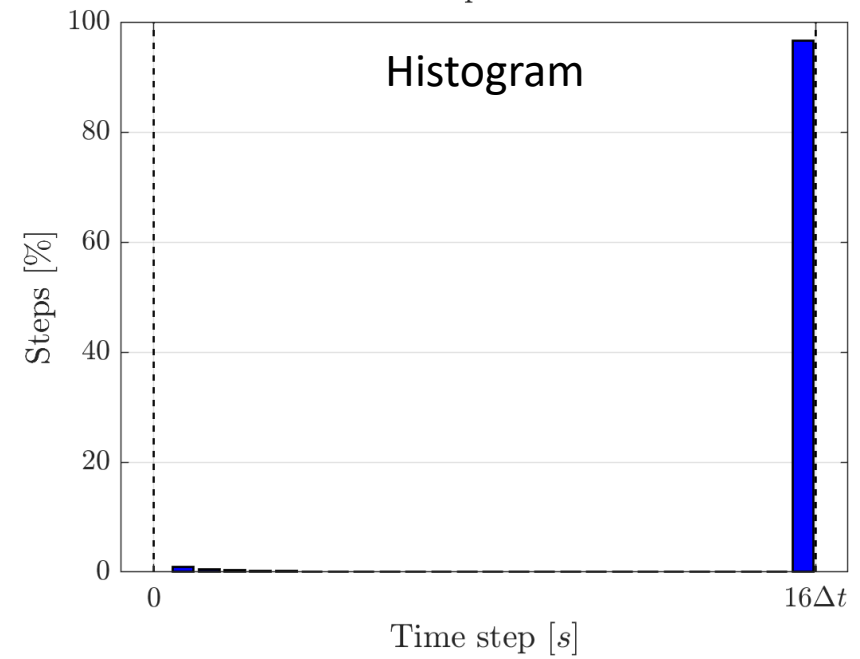
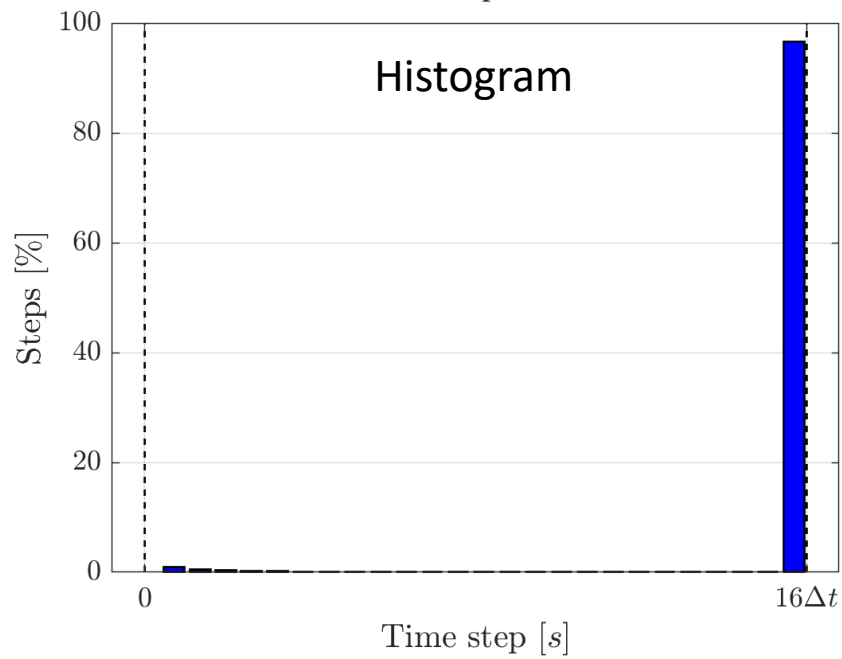
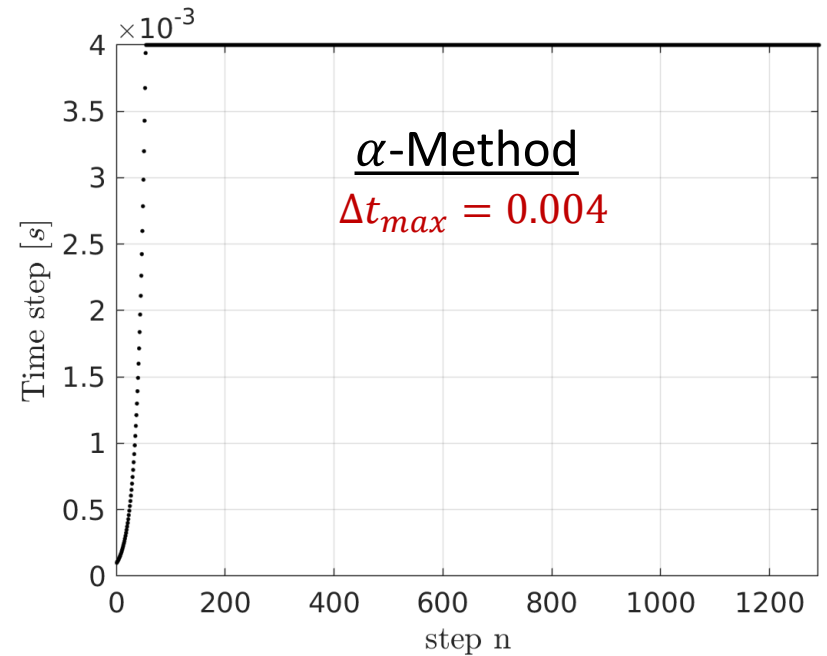
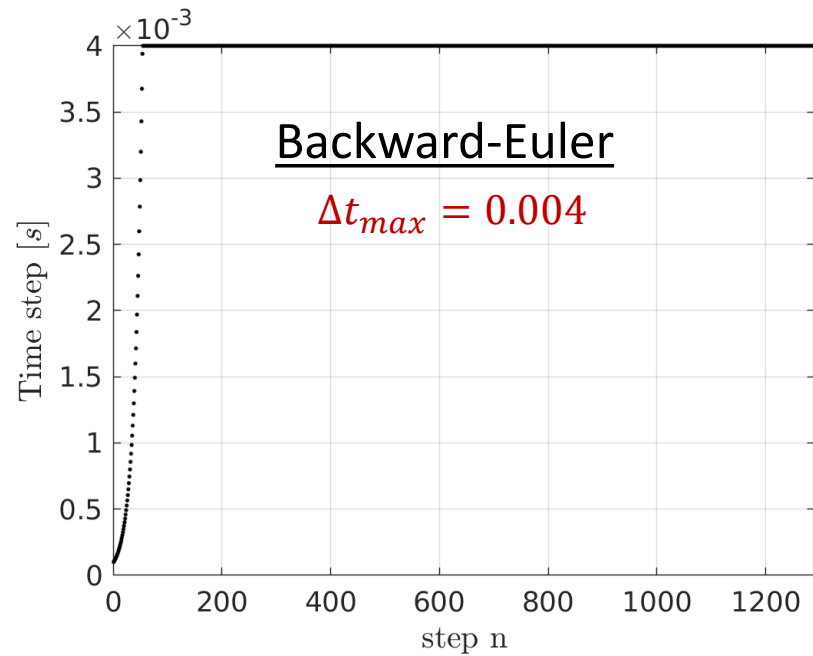
Generally, in this test case, α -Method matches the accuracy of Backward-Euler even using twice the time step of Backward-Euler.

$$\text{error} = \frac{|\max(\mathbf{v}_{\mathbf{x}}) - 1.5|}{1.5} \times 100$$

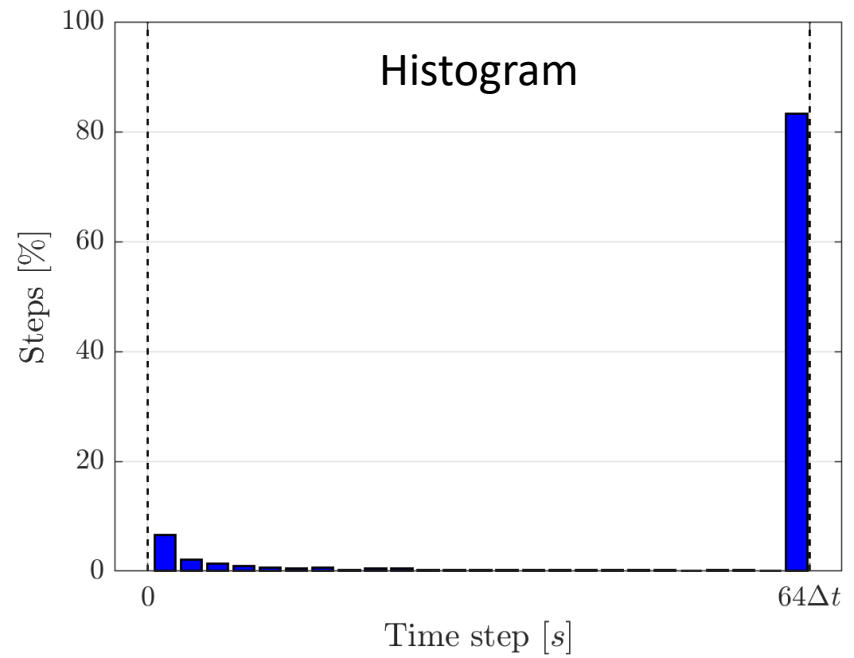
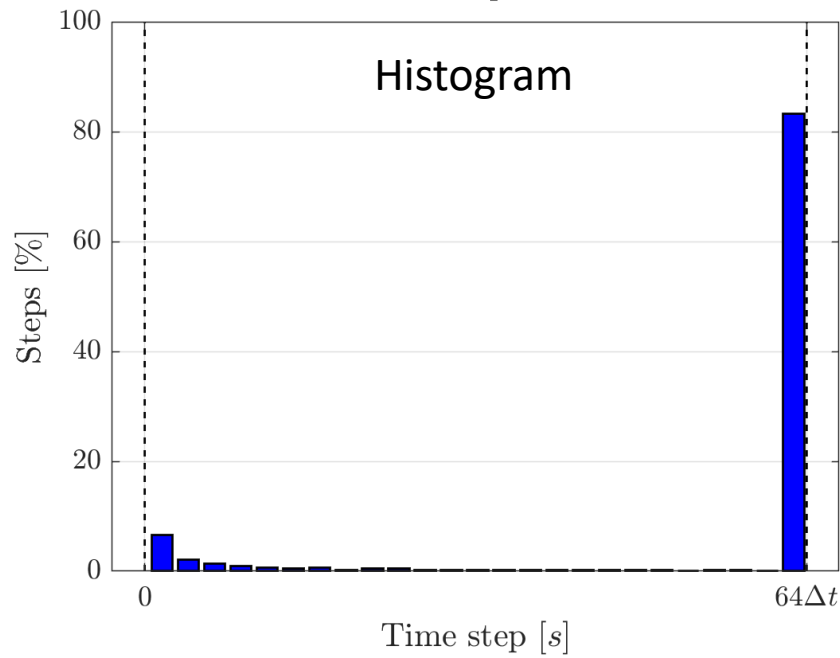
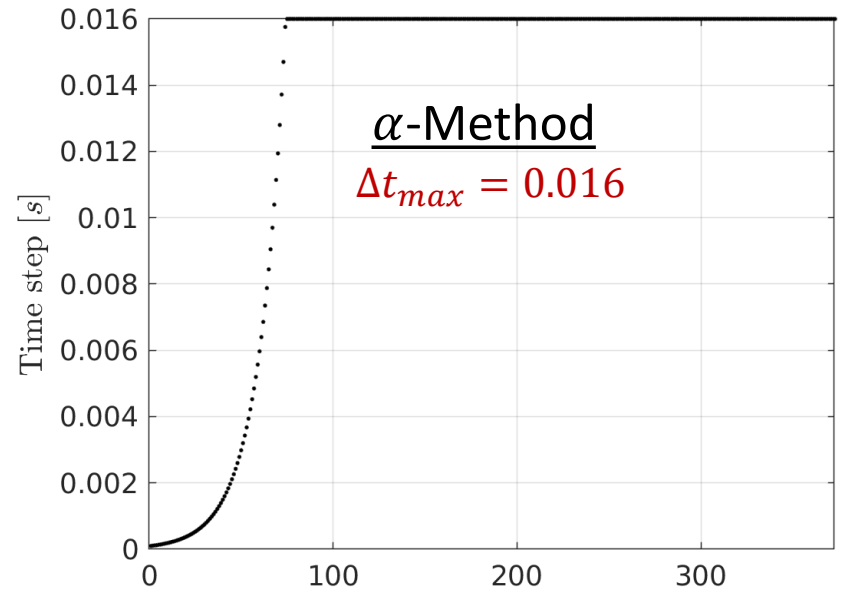
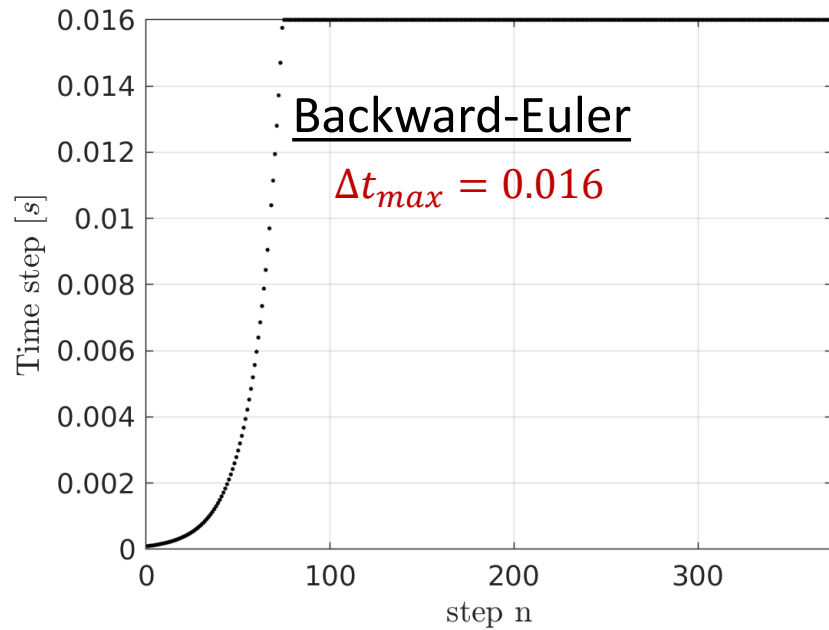
Flow Between 2 plates : Results (BE and α M)



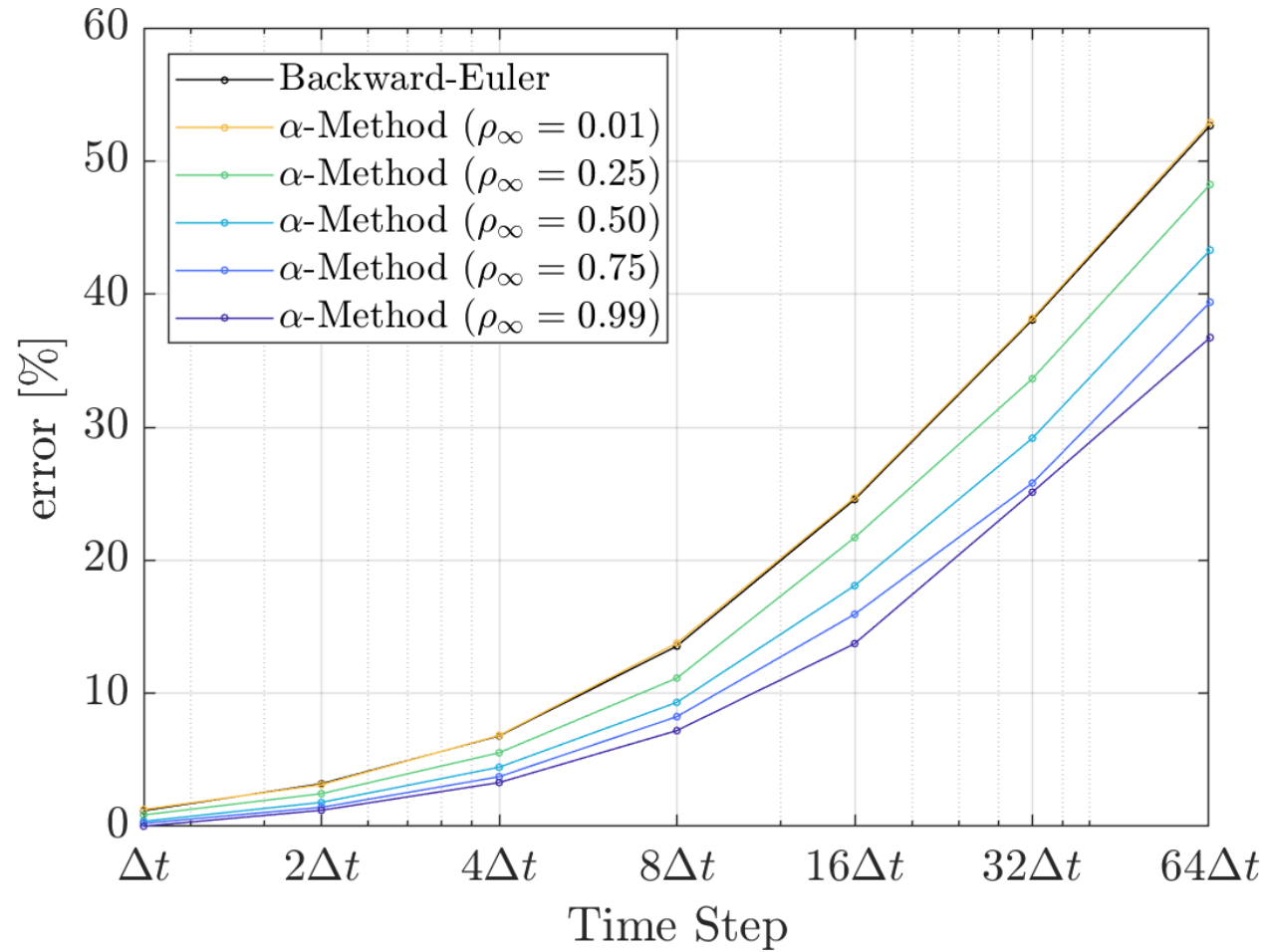
Flow Between 2 plates : Results (BE and α M)



Flow Between 2 plates : Results (BE and α M)



Flow Between 2 plates : Results (BE and $\alpha M(\rho_\infty)$)



Flow around a circular cylinder at $Re = 1000$

Coefficients for comparison:

(Lift Coefficient)

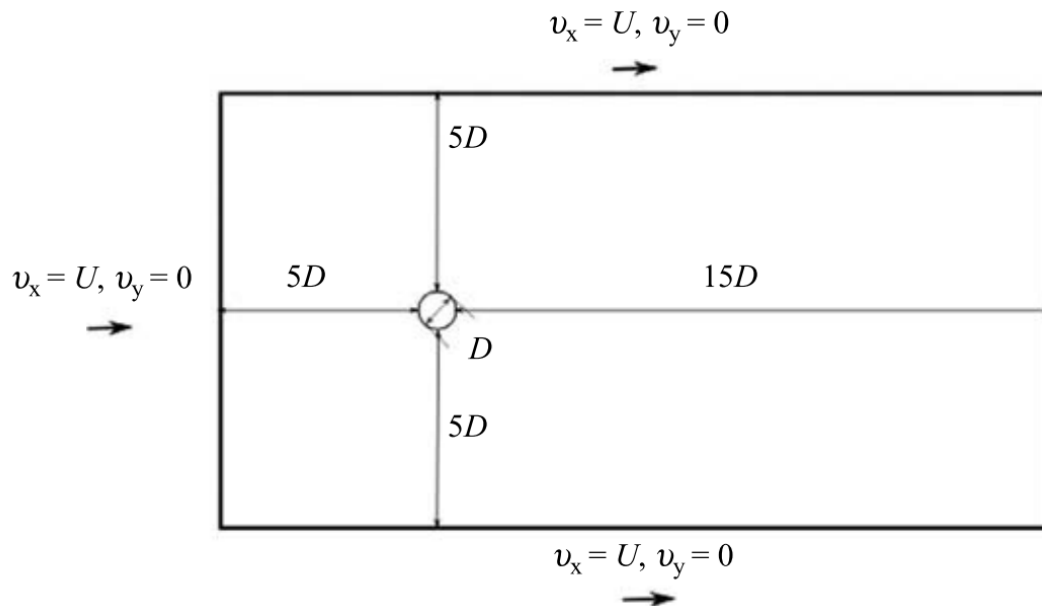
$$C_L(t) = \frac{F_L(t)}{\frac{1}{2}\rho U^2 D}$$

(Drag Coefficient)

$$C_D(t) = \frac{F_D(t)}{\frac{1}{2}\rho U_\infty^2 D}$$

(Strouhal number)

$$St = \frac{fD}{U}$$

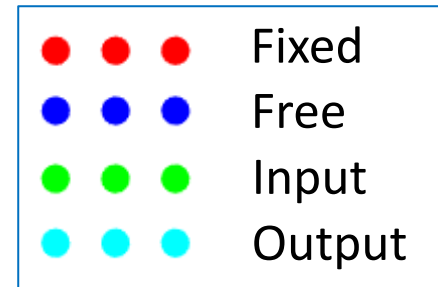
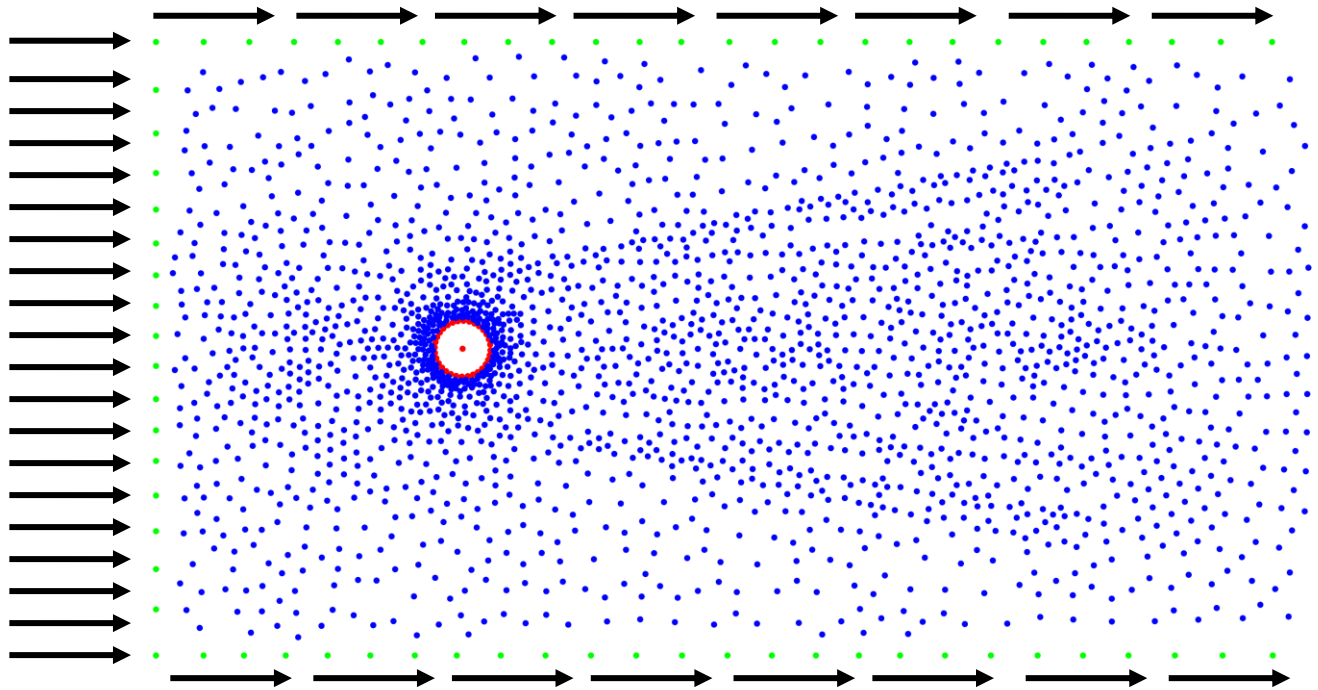


Idelsohn et.al. (2013)

Idelsohn, S. R., Nigro, N. M., Gimenez, J. M., Rossi, R., & Marti, J. M. (2013). A fast and accurate method to solve the incompressible Navier-Stokes equations. Engineering Computations.

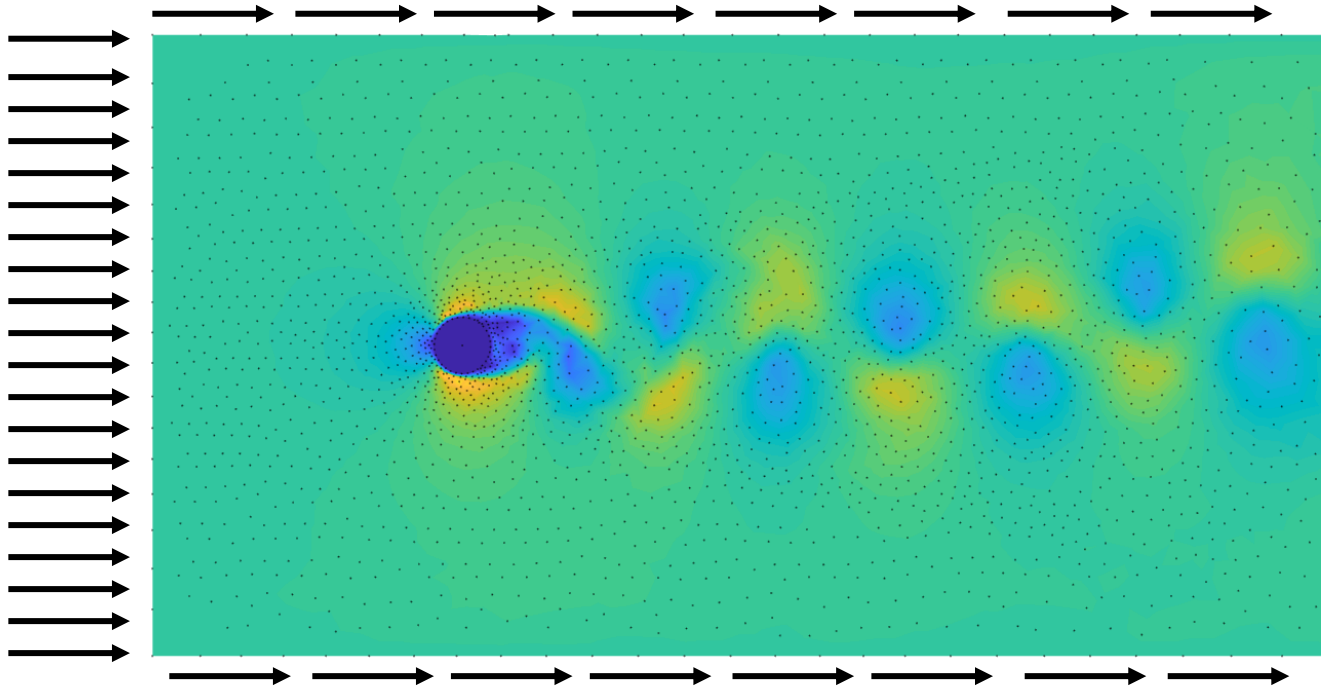
Idelsohn, S., Nigro, N., Limache, A., & Oñate, E. (2012). Large time-step explicit integration method for solving problems with dominant convection. Computer Methods in Applied Mechanics and Engineering, 217, 168-185.

Flow around a circular cylinder



<i>This work</i>		<i>Idelsohn et.al (2013)</i>	<i>Idelsohn et.al (2012)</i>
Num. Initial Particles	: 2200	44520	77000
Input velocity	: 1 m/s	=	=
Density	: 1 kg/m ³	= (I guess)	= (I guess)
Dynamic viscosity	: 0.001 Pa s.	= (I guess)	= (I guess)
Simulation span	: 50 seconds	25 sec.	70 sec.
Maximum time step	: 0.005 / 0.01 / 0.02 / 0.04	0.025	(variable)
Initial time step	: 0.0001	PFEM-2 (Eulerian)	PFEM-2 (Lagrangian)

Flow around a circular cylinder



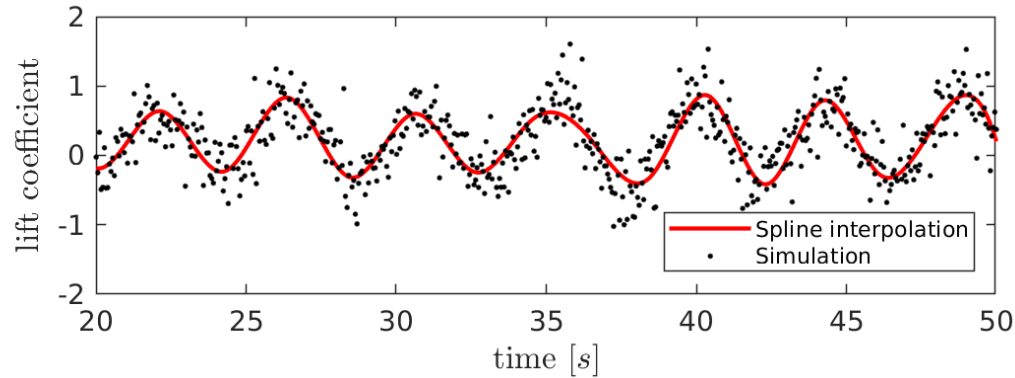
To be compared:

(Strouhal number)

$$S_t = \frac{fD}{U}$$

<i>This work</i>		<i>Idelsohn et.al (2013)</i>	<i>Idelsohn et.al (2012)</i>
Num. Initial Particles	: 2200	44520	77000
Input velocity	: 1 m/s	=	=
Density	: 1 kg/m ³	= (I guess)	= (I guess)
Dynamic viscosity	: 0.001 Pa s.	= (I guess)	= (I guess)
Simulation span	: 50 seconds	25 sec.	70 sec.
Maximum time step	: 0.005 / 0.01 / 0.02 / 0.04	0.025	(variable)
Initial time step	: 0.0001	PFEM-2 (Eulerian)	PFEM-2 (Lagrangian)

Flow around a circular cylinder



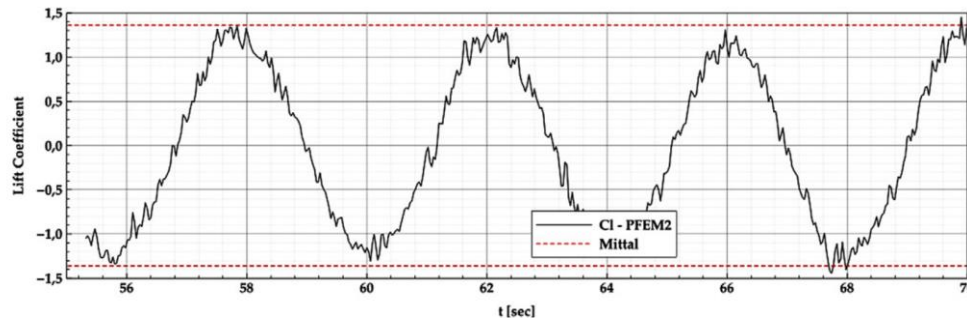
This work

(Strouhal number)

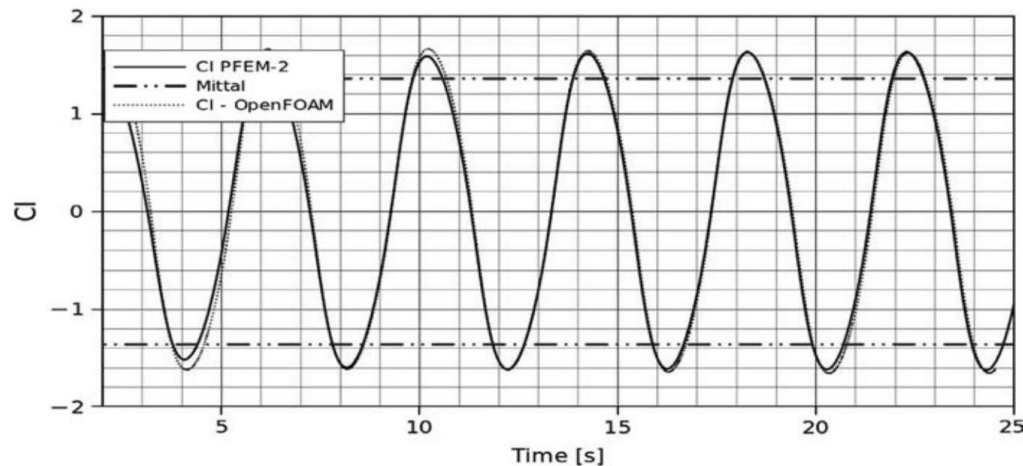
$$S_t = \frac{fD}{U}$$

Where:

$$f = \frac{\text{cycles}}{\text{time period}}$$

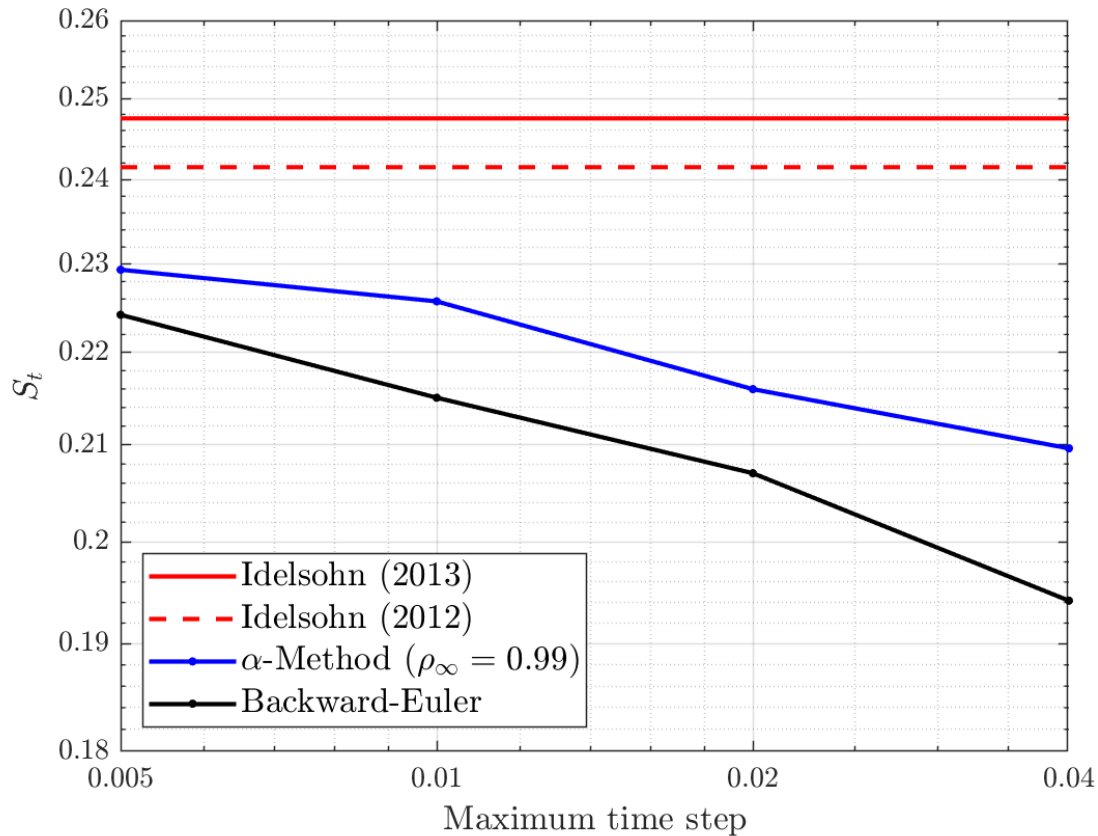


Idelsohn et.al (2012) (Lagrangian) $\Rightarrow S_t = 0.2415$

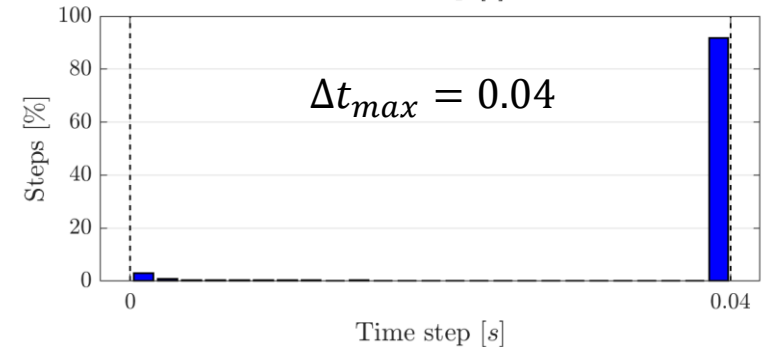
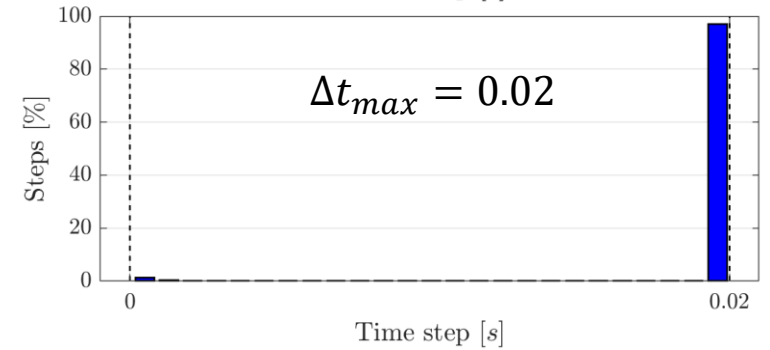
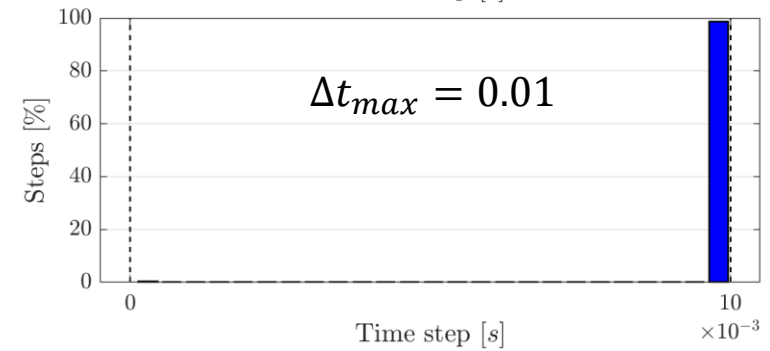
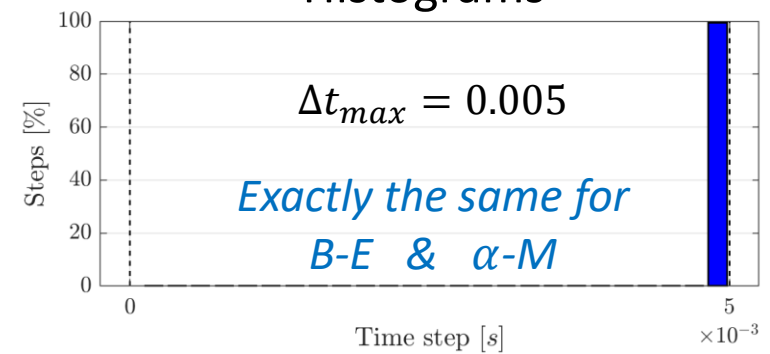


Idelsohn et.al (2013) (Eulerian) $\Rightarrow S_t = 0.2475$

Flow around a circular cylinder



Histograms



1. Time integration in PFEM

2. Results comparison:
Backward-Euler & α -Method

**3. Explicit time integration scheme
used in PFEM-2**

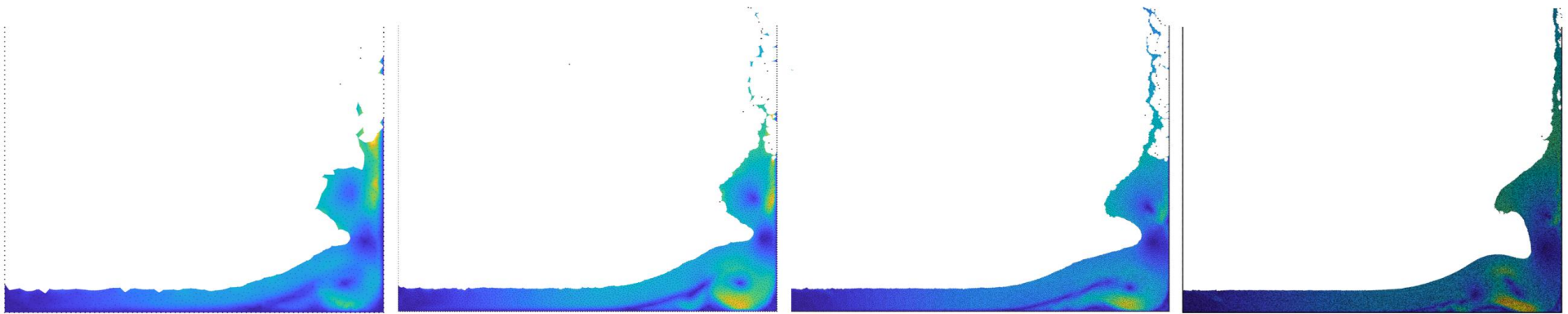
10/05/2021

Study on the explicit time integration used in PFEM-2

Motivation: Search for numerical schemes that allow the use of large time steps.

Study on the explicit time integration used in PFEM-2

Motivation: Search for numerical schemes that allow the use of large time steps.



$$h_{\text{char}} = 0.0073$$

$$N_{\text{part}} = 1000$$

$$\Delta t_{\text{max}} = 0.001$$

$$N_{\text{steps}} = 783$$

$$h_{\text{char}} = 0.00365$$

$$N_{\text{part}} = 3600$$

$$\Delta t_{\text{max}} = 0.001$$

$$N_{\text{steps}} = 969$$

$$h_{\text{char}} = 0.001825$$

$$N_{\text{part}} = 13600$$

$$\Delta t_{\text{max}} = 0.001$$

$$N_{\text{steps}} = 1385$$

$$h_{\text{char}} = 0.0009125$$

$$N_{\text{part}} = 52800$$

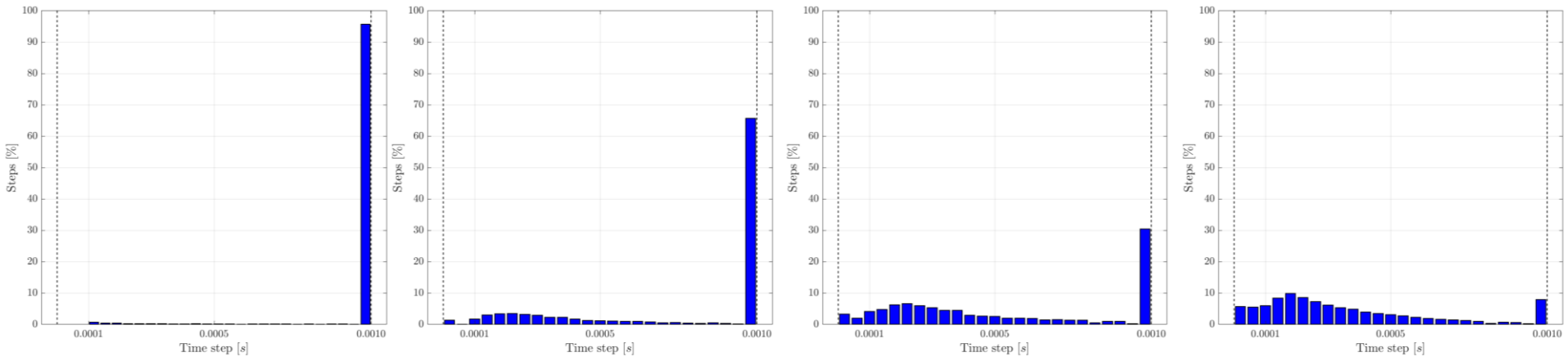
$$\Delta t_{\text{max}} = 0.001$$

$$N_{\text{steps}} = 2126$$

(Using Backward-Euler)

Study on the explicit time integration used in PFEM-2

Motivation: Search for numerical schemes that allow the use of large time steps.



$$h_{\text{char}} = 0.0073$$

$$h_{\text{char}} = 0.00365$$

$$h_{\text{char}} = 0.001825$$

$$h_{\text{char}} = 0.0009125$$

$$N_{\text{part}} = 1000$$

$$N_{\text{part}} = 3600$$

$$N_{\text{part}} = 13600$$

$$N_{\text{part}} = 52800$$

$$\Delta t_{\text{max}} = 0.001$$

$$\Delta t_{\text{max}} = 0.001$$

$$\Delta t_{\text{max}} = 0.001$$

$$\Delta t_{\text{max}} = 0.001$$

$$N_{\text{steps}} = 783$$

$$N_{\text{steps}} = 969$$

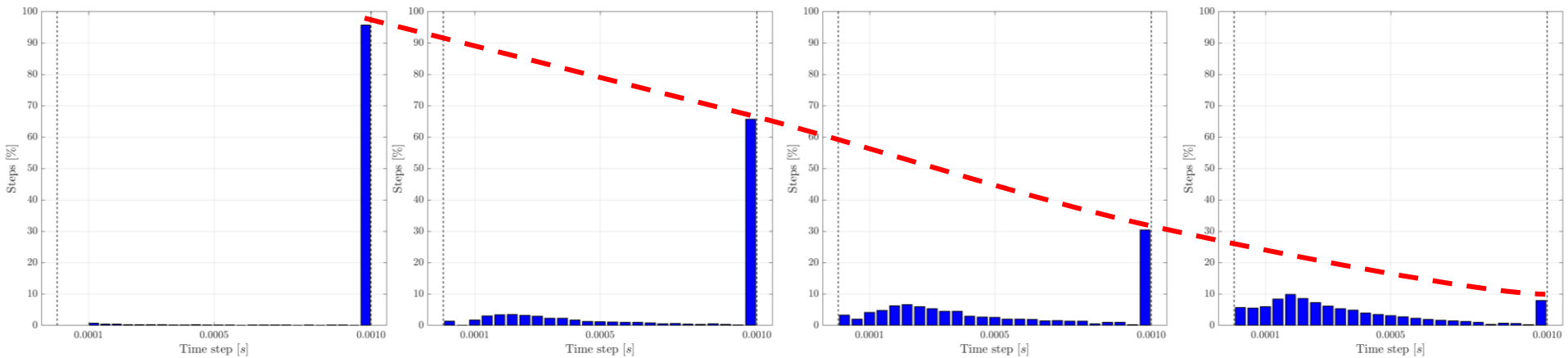
$$N_{\text{steps}} = 1385$$

$$N_{\text{steps}} = 2126$$

(Using Backward-Euler)

Study on the explicit time integration used in PFEM-2

Motivation: Search for numerical schemes that allow the use of large time steps.



$$h_{\text{char}} = 0.0073$$

$$h_{\text{char}} = 0.00365$$

$$h_{\text{char}} = 0.001825$$

$$h_{\text{char}} = 0.0009125$$

$$N_{\text{part}} = 1000$$

$$N_{\text{part}} = 3600$$

$$N_{\text{part}} = 13600$$

$$N_{\text{part}} = 52800$$

$$\Delta t_{\text{max}} = 0.001$$

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$$\Delta t_{\text{max}} = 0.001$$

$$N_{\text{steps}} = 783$$

$$N_{\text{steps}} = 969$$

$$N_{\text{steps}} = 1385$$

$$N_{\text{steps}} = 2126$$

(Using Backward-Euler)

Study on the explicit time integration used in PFEM-2

Known: \mathbf{x}_n , \mathbf{v}_n , $\dot{\mathbf{v}}_n$

1) Set $k = 0$

2) Initial guess: $\mathbf{x}_k = \mathbf{x}_n$

3) *While* (convergence is not reached)

3.1) Compute:

$$\mathbf{A}_{BE}(\mathbf{x}_k, \mathbf{v}_k)$$

$$\mathbf{b}_{BE}(\mathbf{x}_k, \mathbf{v}_n, \mathbf{v}_k)$$

3.2) Solve : $\mathbf{A}_{BE} \mathbf{q}_{n+1} = \mathbf{b}_{BE}$

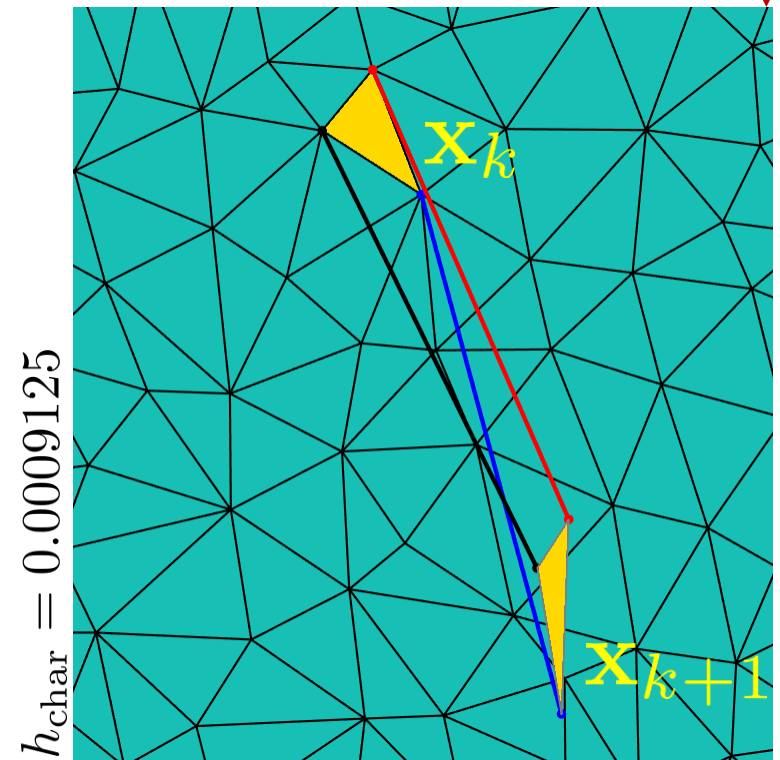
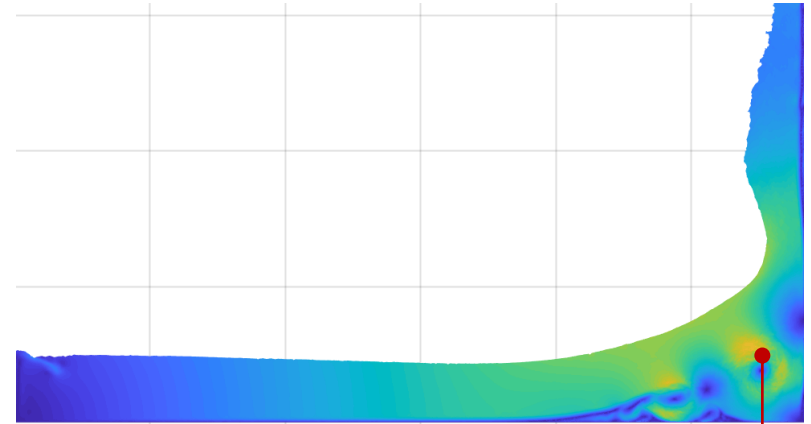
3.3) Update : $\mathbf{x}_k = \mathbf{x}_n + \Delta t \mathbf{v}_{k+1}$

3.4) Set : $k = k + 1$

4) Set : $\mathbf{q}_{n+1} = \mathbf{q}_k$

Update : $\mathbf{x}_{n+1} = \mathbf{x}_n + \Delta t \mathbf{v}_{n+1}$

5) **RE-MESH** (if necessary)



Study on the explicit time integration used in PFEM-2

Known: \mathbf{x}_n , \mathbf{v}_n , $\dot{\mathbf{v}}_n$

1) Set $k = 0$

2) Initial guess: $\mathbf{x}_k = \mathbf{x}_n$

3) *While* (convergence is not reached)

3.1) Compute:

$$\mathbf{A}_{\text{BE}}(\mathbf{x}_k, \mathbf{v}_k)$$

$$\mathbf{b}_{\text{BE}}(\mathbf{x}_k, \mathbf{v}_n, \mathbf{v}_k)$$

3.2) Solve : $\mathbf{A}_{\text{BE}} \mathbf{q}_{n+1} = \mathbf{b}_{\text{BE}}$

3.3) Update : $\mathbf{x}_k = \mathbf{x}_n + \Delta t \mathbf{v}_{k+1}$

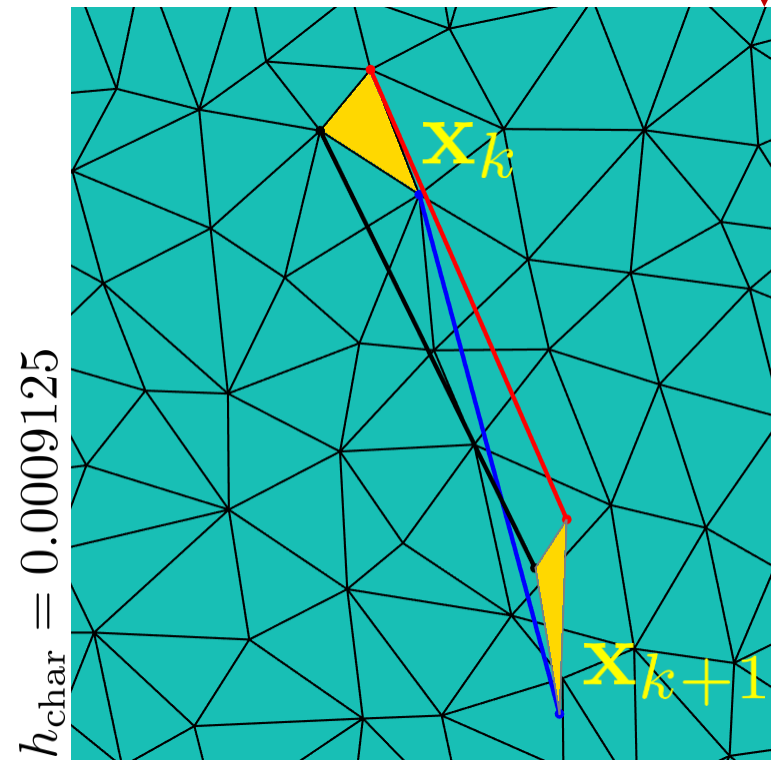
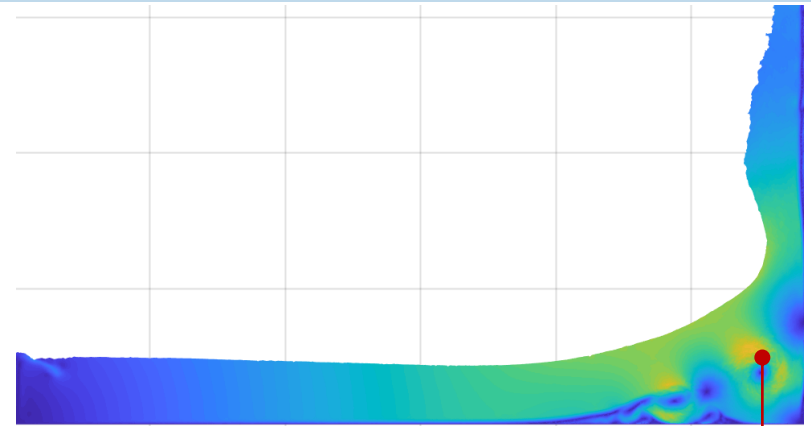
+ RE-MESH (if necessary)

3.4) Set : $k = k + 1$

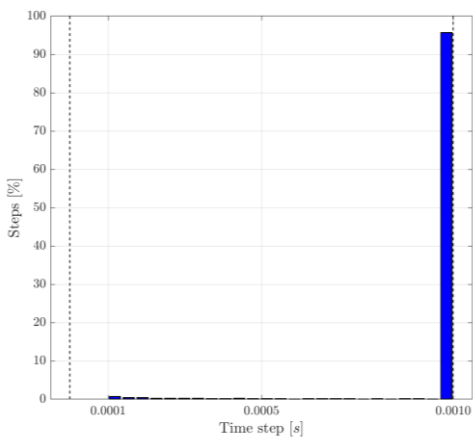
4) Set : $\mathbf{q}_{n+1} = \mathbf{q}_k$

Update : $\mathbf{x}_{n+1} = \mathbf{x}_n + \Delta t \mathbf{v}_{n+1}$

5) RE-MESH (if necessary)

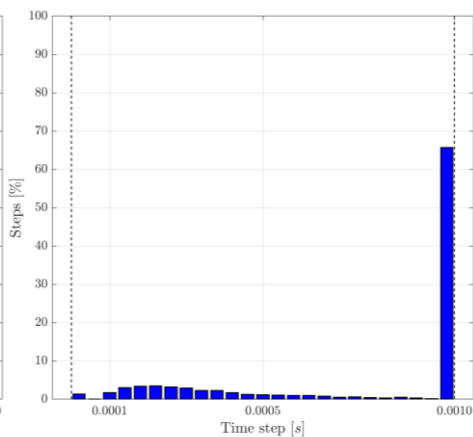


Study on the explicit time integration used in PFEM-2



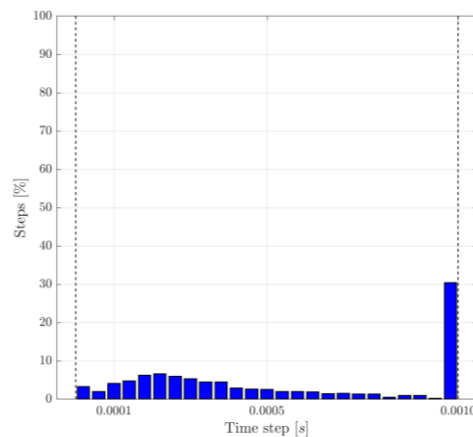
$$h_{\text{char}} = 0.0073$$

$$N_{\text{steps}} = 783$$



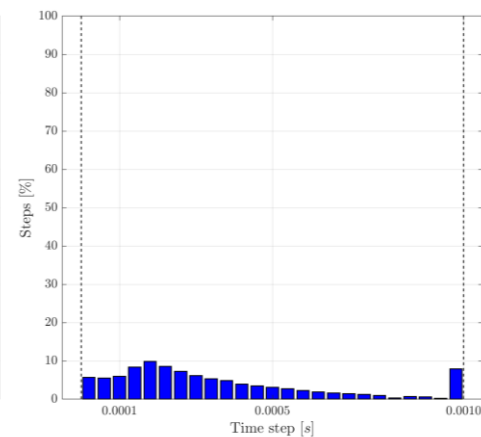
$$h_{\text{char}} = 0.00365$$

$$N_{\text{steps}} = 969$$



$$h_{\text{char}} = 0.001825$$

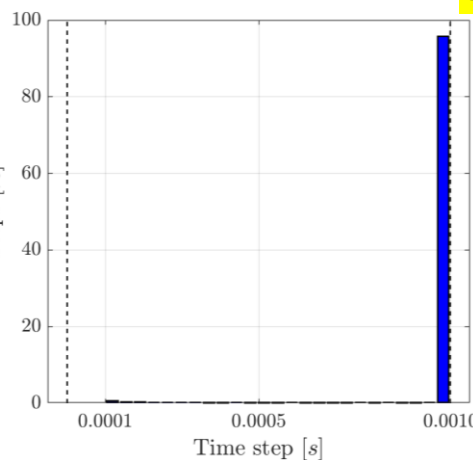
$$N_{\text{steps}} = 1385$$



$$h_{\text{char}} = 0.0009125$$

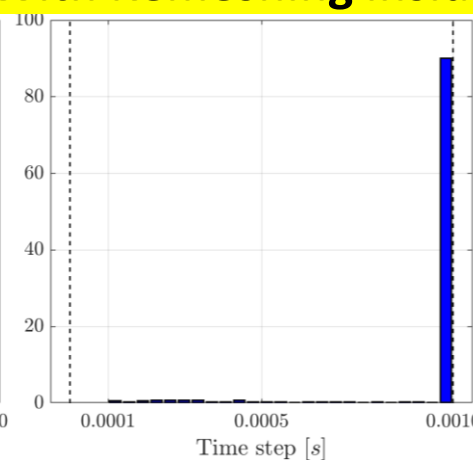
$$N_{\text{steps}} = 2126$$

With Remeshing inside non-linear algorithm



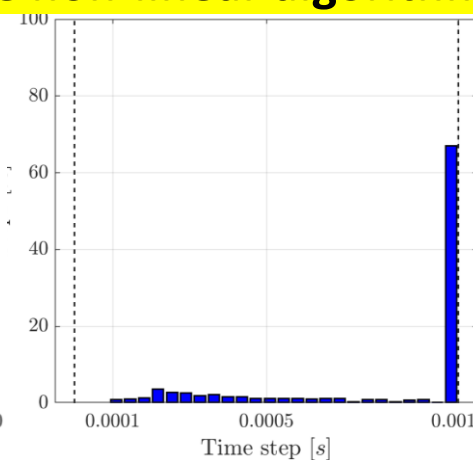
$$h_{\text{char}} = 0.0073$$

$$N_{\text{steps}} = 771$$



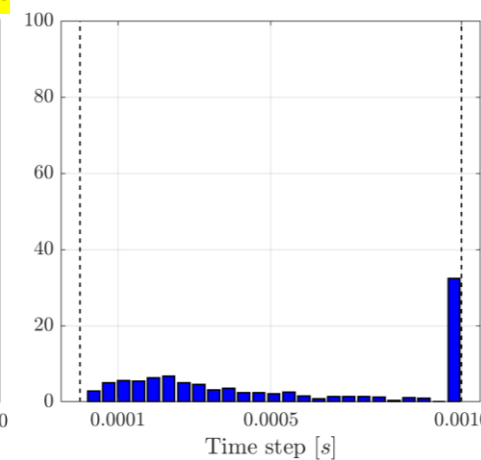
$$h_{\text{char}} = 0.00365$$

$$N_{\text{steps}} = 798$$



$$h_{\text{char}} = 0.001825$$

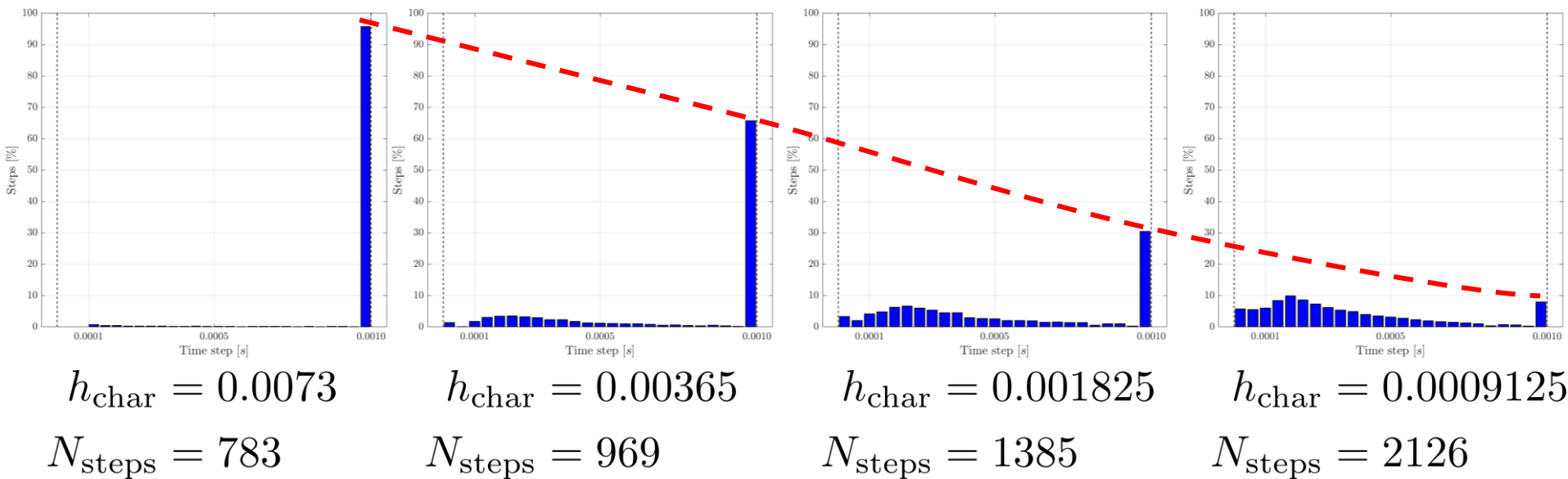
$$N_{\text{steps}} = 943$$



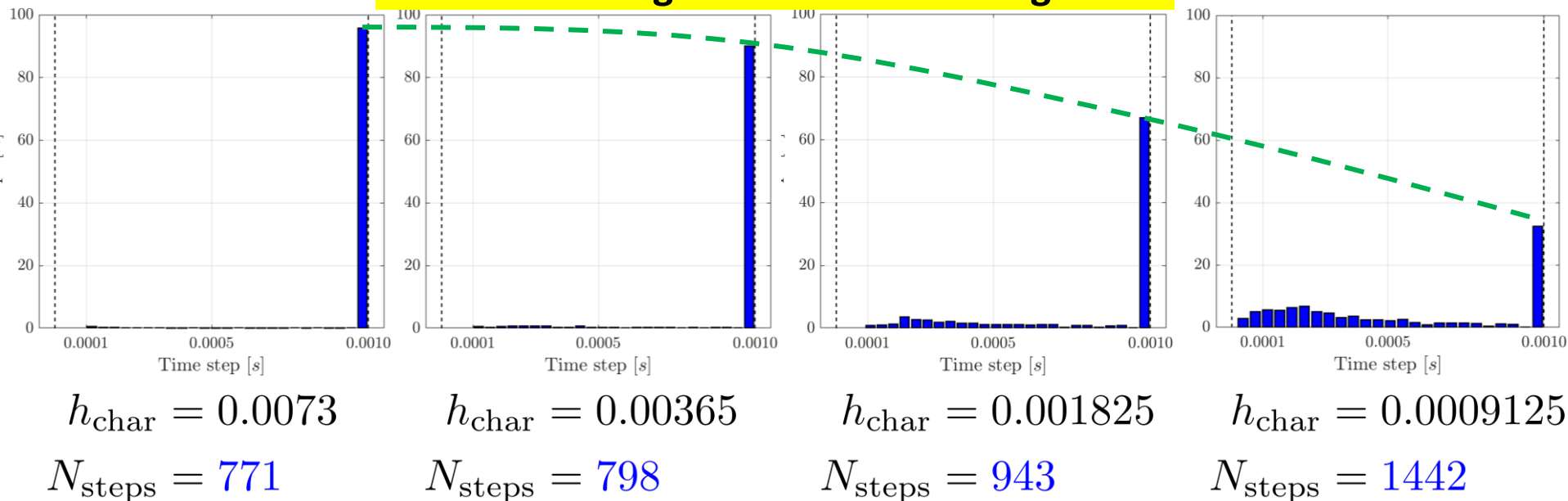
$$h_{\text{char}} = 0.0009125$$

$$N_{\text{steps}} = 1442$$

Study on the explicit time integration used in PFEM-2



With Remeshing inside non-linear algorithm



Study on the explicit time integration used in PFEM-2

Known: \mathbf{x}_n , \mathbf{v}_n , $\dot{\mathbf{v}}_n$

1) Set $k = 0$

2) Initial guess: $\mathbf{x}_k = \mathbf{x}_n$

3) *While* (convergence is not reached)

3.1) Compute:

$$\mathbf{A}_{\text{BE}}(\mathbf{x}_k, \mathbf{v}_k)$$

$$\mathbf{b}_{\text{BE}}(\mathbf{x}_k, \mathbf{v}_n, \mathbf{v}_k)$$

3.2) Solve : $\mathbf{A}_{\text{BE}} \mathbf{q}_{n+1} = \mathbf{b}_{\text{BE}}$

3.3) Update : $\mathbf{x}_k = \mathbf{x}_n + \Delta t \mathbf{v}_{k+1}$

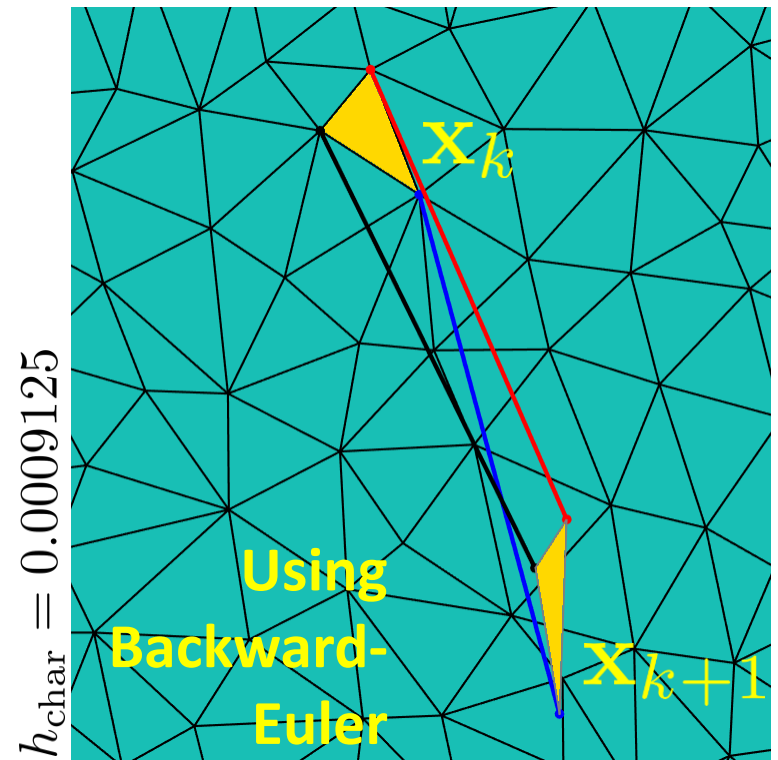
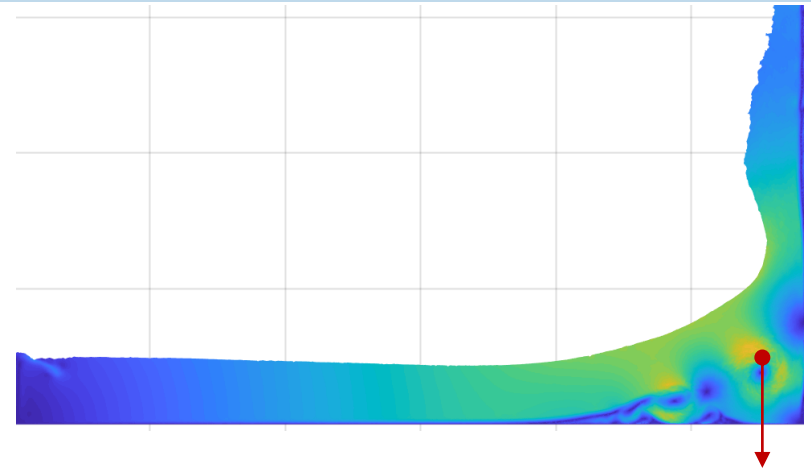
+ RE-MESH (if necessary)

3.4) Set : $k = k + 1$

4) Set : $\mathbf{q}_{n+1} = \mathbf{q}_k$

Update : $\mathbf{x}_{n+1} = \mathbf{x}_n + \Delta t \mathbf{v}_{n+1}$

5) RE-MESH (if necessary)



Study on the explicit time integration used in PFEM-2

Known: \mathbf{x}_n , \mathbf{v}_n , $\dot{\mathbf{v}}_n$

1) Set $k = 0$

2) Initial guess: $\mathbf{x}_k = \mathbf{x}_n$

3) *While* (convergence is not reached)

3.1) Compute:

$$\mathbf{A}_{\text{BE}}(\mathbf{x}_k, \mathbf{v}_k)$$

$$\mathbf{b}_{\text{BE}}(\mathbf{x}_k, \mathbf{v}_n, \mathbf{v}_k)$$

3.2) Solve : $\mathbf{A}_{\text{BE}} \mathbf{q}_{n+1} = \mathbf{b}_{\text{BE}}$

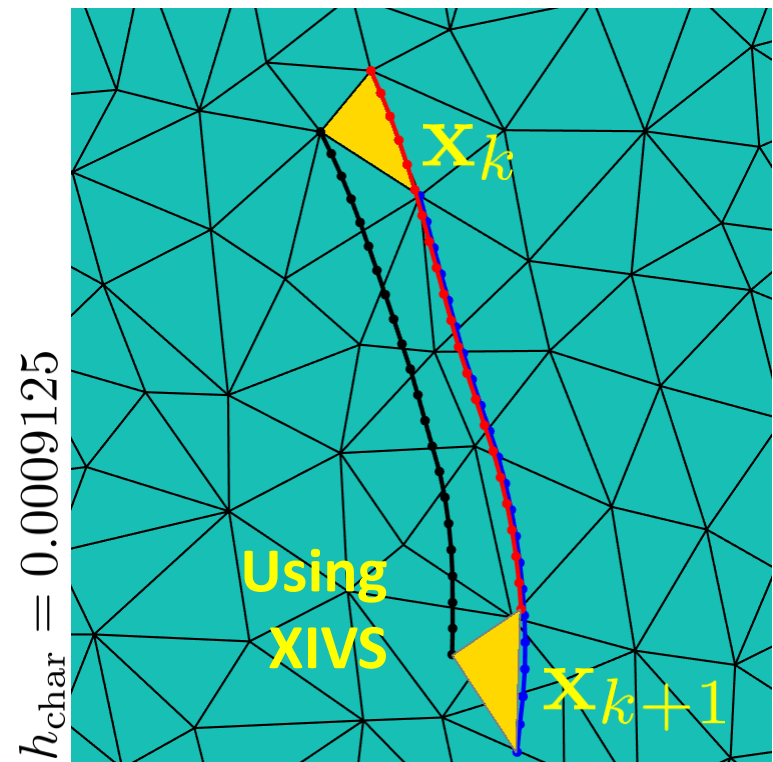
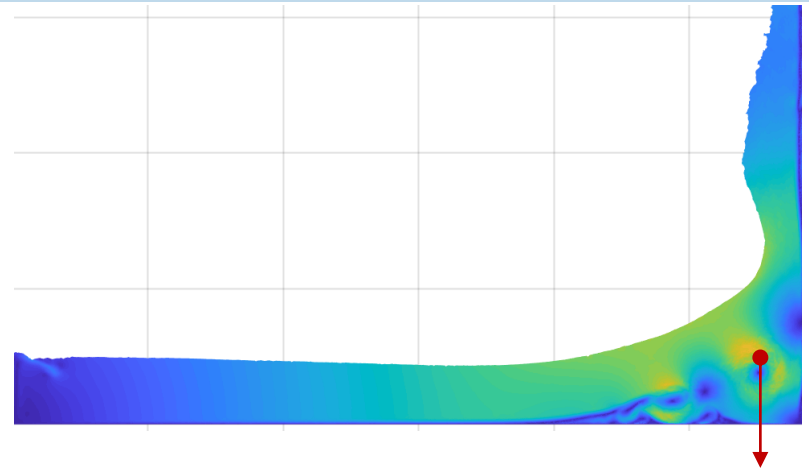
3.3) Update : $\mathbf{x}_k \rightarrow$ Use a more accurate
Integration scheme
+ RE-MESH (if necessary)

3.4) Set : $k = k + 1$

4) Set : $\mathbf{q}_{n+1} = \mathbf{q}_k$

Update : $\mathbf{x}_{n+1} = \mathbf{x}_n + \Delta t \mathbf{v}_{n+1}$

5) RE-MESH (if necessary)



Study on the explicit time integration used in PFEM-2

$$\mathbf{v}_{n+1}(\mathbf{x}_{n+1}^p) = \mathbf{v}_n(\mathbf{x}_n^p) + \int_{t_n}^{t_{n+1}} \dot{\mathbf{v}}(\tau, \mathbf{x}_\tau^p) d\tau \quad (1)$$

$$\mathbf{x}_{n+1}^p = \mathbf{x}_n^p + \int_{t_n}^{t_{n+1}} \mathbf{v}(\tau, \mathbf{x}_\tau^p) d\tau \quad (2)$$

2) Assume $\dot{\mathbf{v}}(\tau, \mathbf{x}_\tau^p)$ constant between $[t_n, t_{n+1}]$ ~~and around \mathbf{x}^p~~

See, for instance:

Dialami, N., Chiumenti, M., Cervera, M., De Saracibar, C. A., & Ponthot, J. P. (2015). Material flow visualization in friction stir welding via particle tracing. *International Journal of Material Forming*, 8(2), 167-181.

Marti, J., & Ryzhakov, P. (2020). Improving accuracy of the moving grid particle finite element method via a scheme based on Strang splitting. *Computer Methods in Applied Mechanics and Engineering*, 369, 113212.

Idelsohn, S., Nigro, N., Limache, A., & Oñate, E. (2012). Large time-step explicit integration method for solving problems with dominant convection. *Computer Methods in Applied Mechanics and Engineering*, 217, 168-185.

Study on the explicit time integration used in PFEM-2

$$\mathbf{v}_{n+1}(\mathbf{x}_{n+1}^p) = \mathbf{v}_n(\mathbf{x}_n^p) + \int_{t_n}^{t_{n+1}} \dot{\mathbf{v}}(\tau, \mathbf{x}_\tau^p) d\tau \quad (1)$$

$$\mathbf{x}_{n+1}^p = \mathbf{x}_n^p + \int_{t_n}^{t_{n+1}} \mathbf{v}(\tau, \mathbf{x}_\tau^p) d\tau \quad (2)$$

2) Assume $\dot{\mathbf{v}}(\tau, \mathbf{x}_\tau^p)$ constant between $[t_n, t_{n+1}]$ ~~and around \mathbf{x}^p~~

2.a) Assume $\dot{\mathbf{v}}(\tau, \mathbf{x}_\tau^p) = \dot{\mathbf{v}}(t_n, \mathbf{x}_\tau^p) = \dot{\mathbf{v}}_n(\mathbf{x}_\tau^p)$

$$\mathbf{v}_{n+1}(\mathbf{x}_{n+1}^p) = \mathbf{v}_n(\mathbf{x}_n^p) + \int_{t_n}^{t_{n+1}} \dot{\mathbf{v}}_n(\mathbf{x}_\tau^p) d\tau \quad (3)$$

Space
Discretization:

$$\mathbf{v}_{n+1}(\mathbf{x}_{n+1}^p) = \mathbf{v}_n(\mathbf{x}_n^p) + \int_{t_n}^{t_{n+1}} N_I(\mathbf{x}_\tau^p) \dot{\mathbf{v}}_{n,I} d\tau \quad (4)$$

Study on the explicit time integration used in PFEM-2

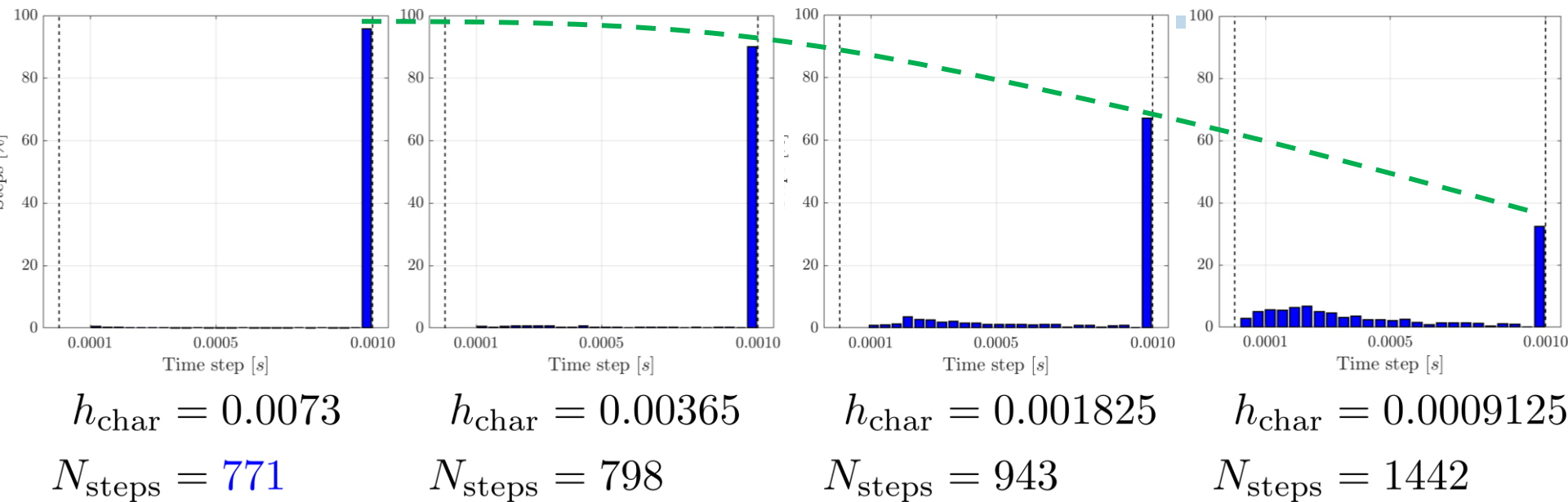
Time
Discretization:

$$\mathbf{v}_{n+1}(\mathbf{x}_{n+1}^p) = \mathbf{v}_n(\mathbf{x}_n^p) + \sum_{i=1}^m \delta t N_I(\mathbf{x}_{n+\frac{i}{m}}^p) \dot{\mathbf{v}}_{n,I} \quad (5)$$

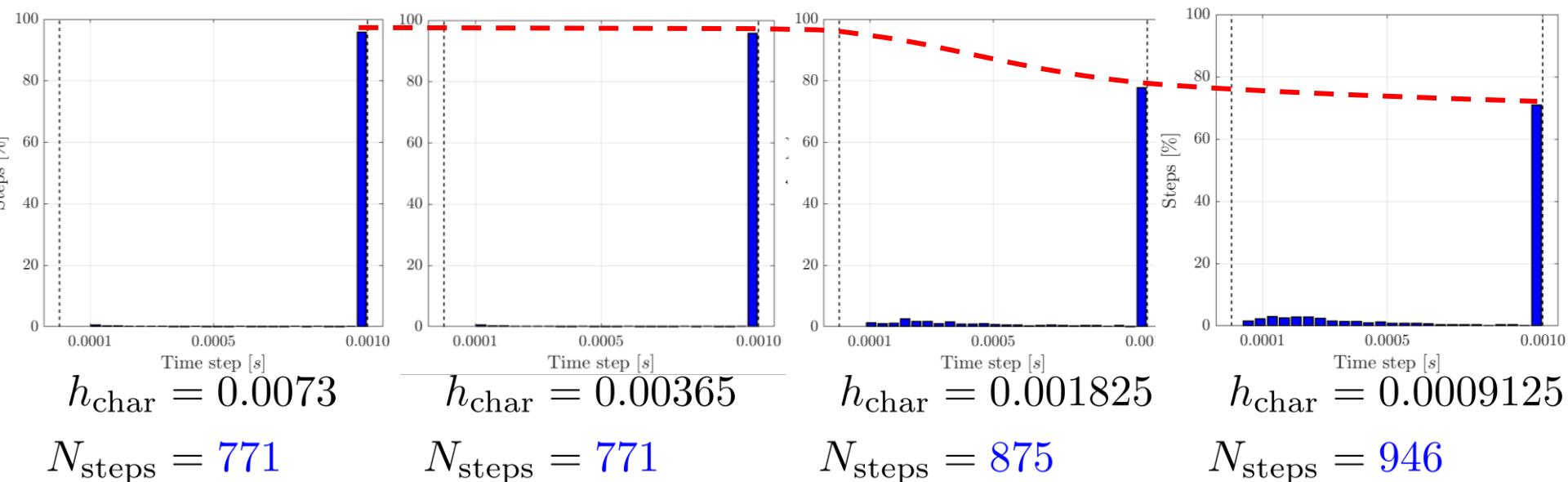
Where : m is the number of sub-steps discretizing the time step Δt

δt is the sub-time step computed as : $\delta t = \frac{\Delta t}{m}$

With Remeshing inside non-linear algorithm

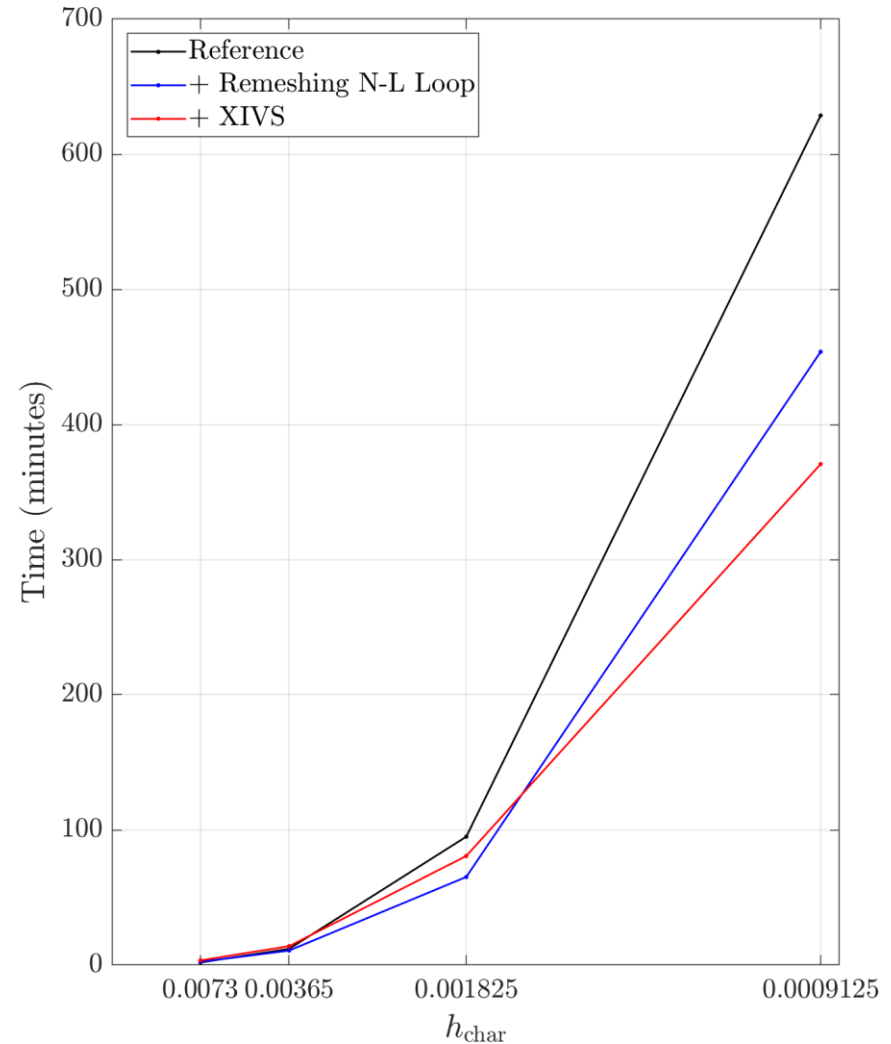
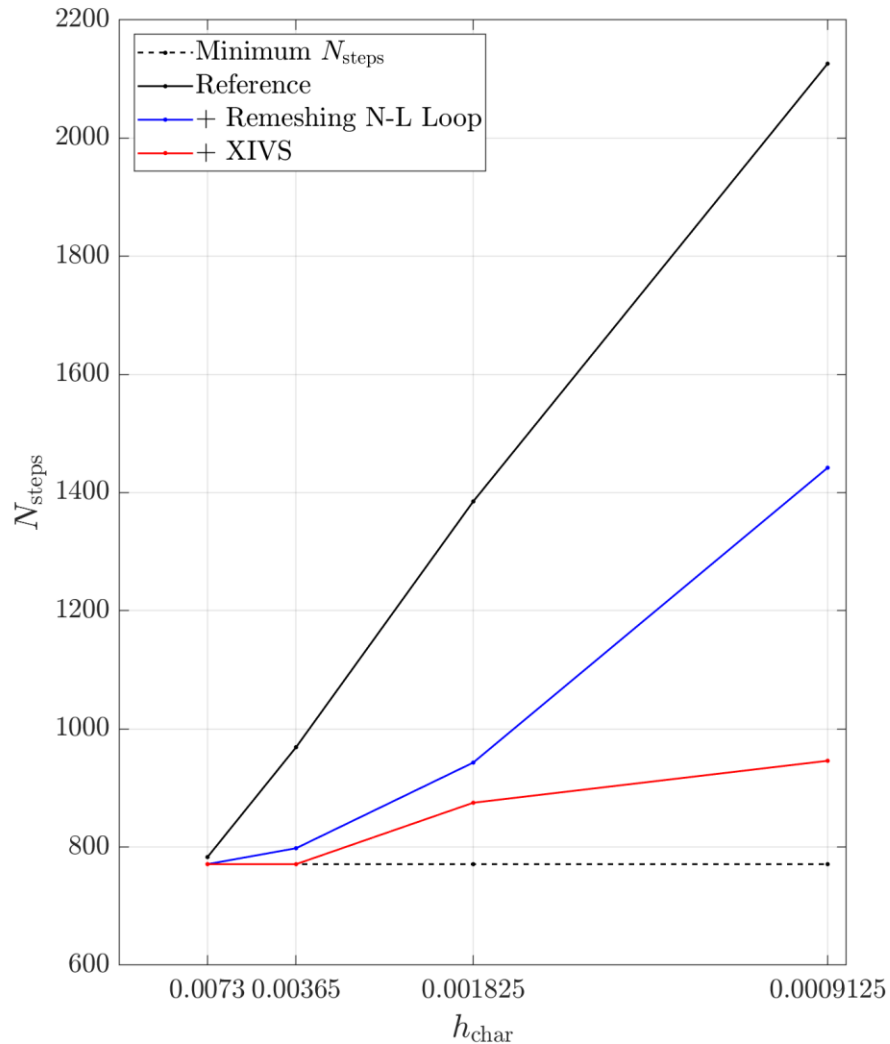


With Remeshing inside non-linear algorithm + more accurate Integration (for position)

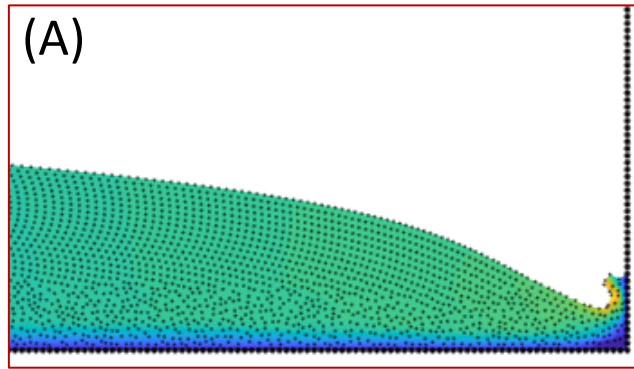


Study on the explicit time integration used in PFEM-2

From Dam Break:



Study on the explicit time integration used in PFEM-2

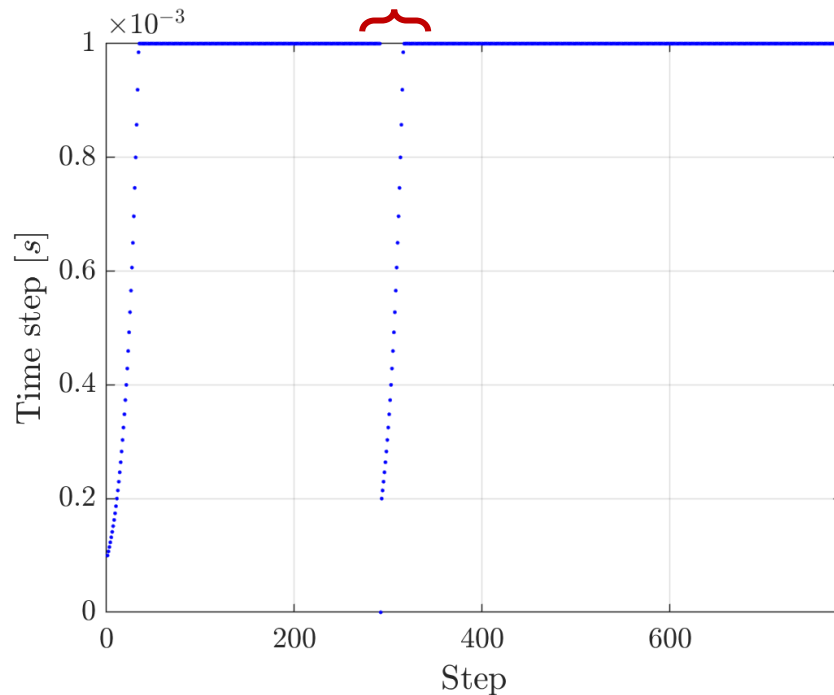


Reference

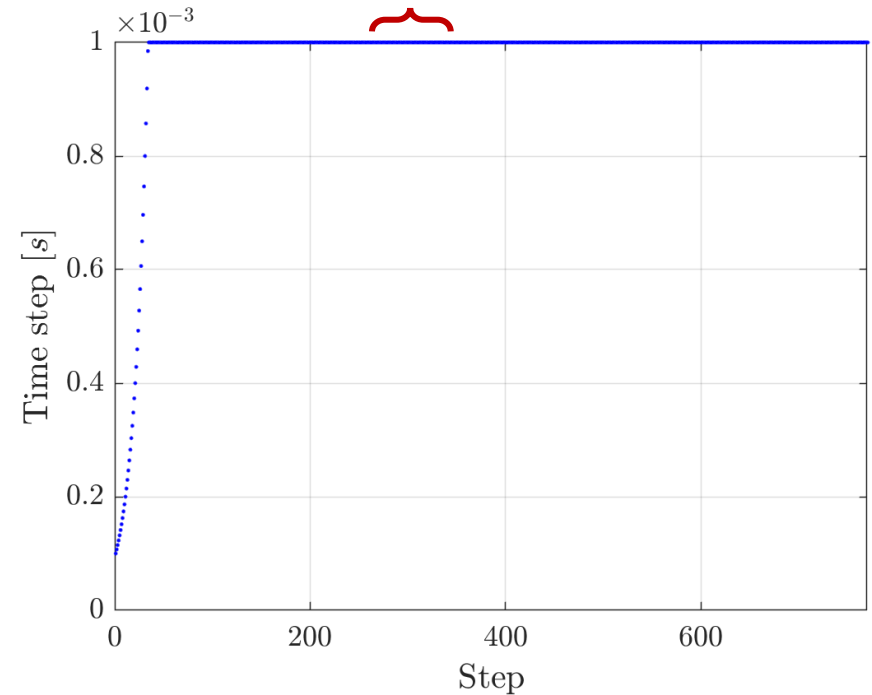
($h_{\text{char}} = 0.0073$)

+ Remeshing (N-L loop)
+ XIVS integration

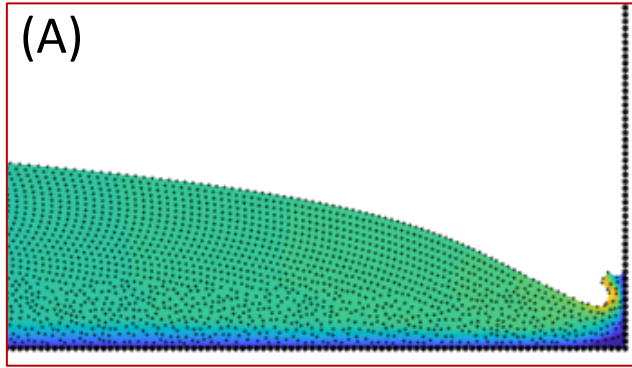
(A)



(A)

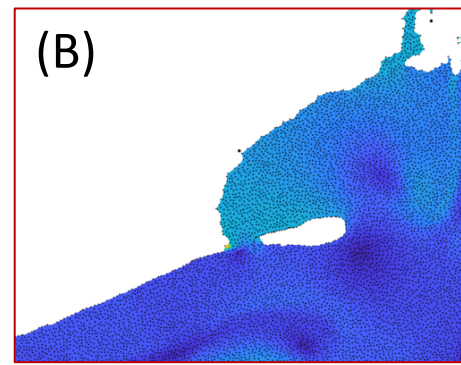


Study on the explicit time integration used in PFEM-2

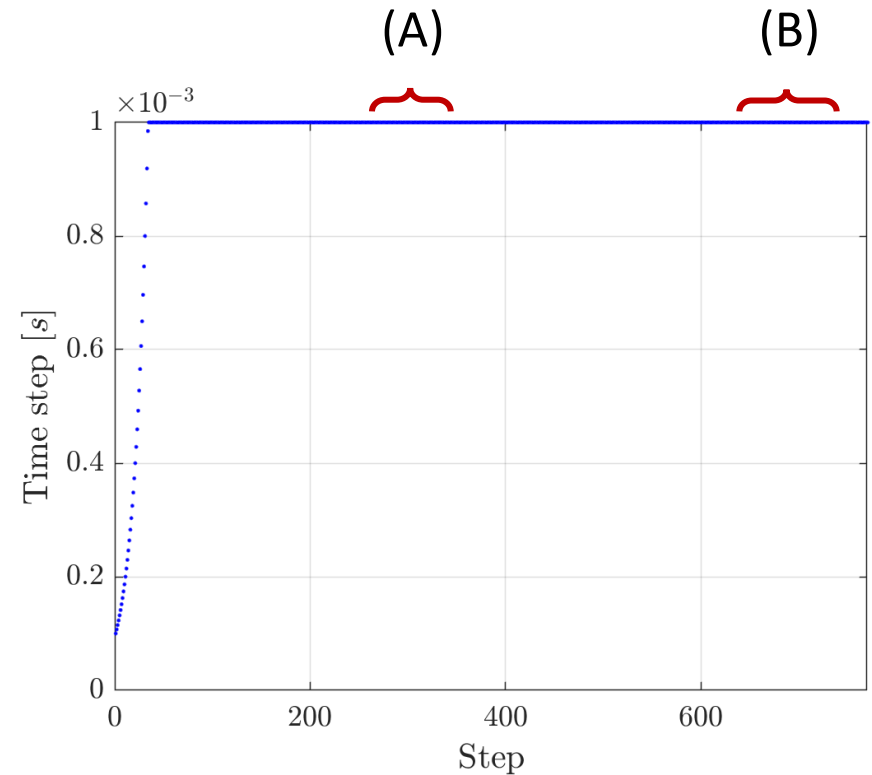
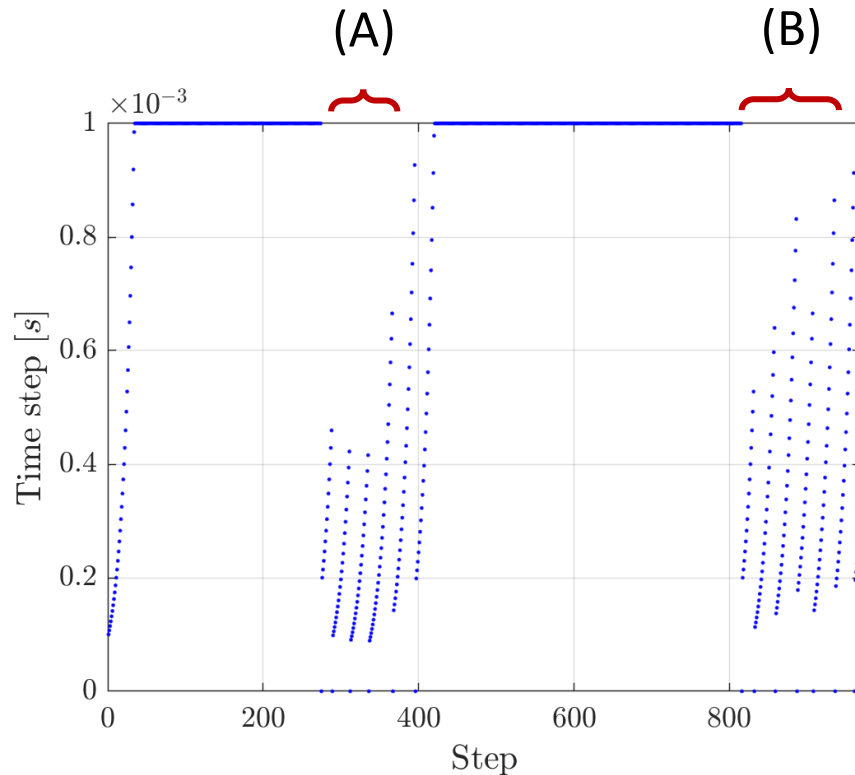


Reference

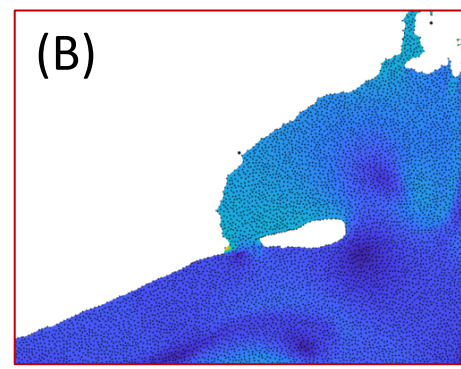
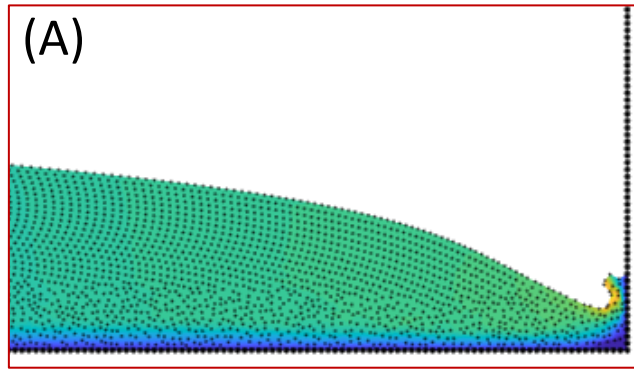
($h_{\text{char}} = 0.00365$)



+ Remeshing (N-L loop)
+ XIVS integration



Study on the explicit time integration used in PFEM-2



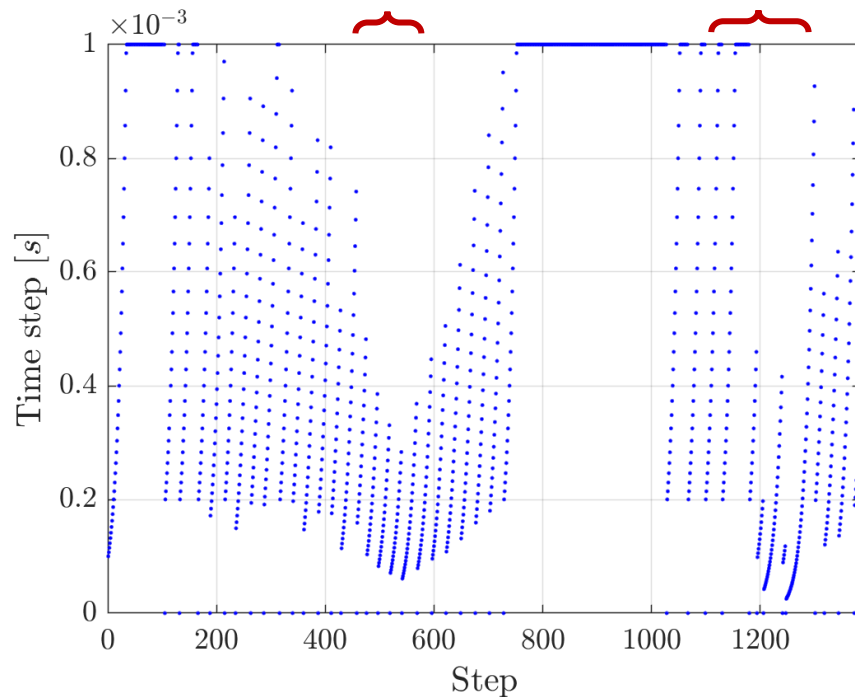
Reference

($h_{\text{char}} = 0.001825$)

+ Remeshing (N-L loop)
+ XIVS integration

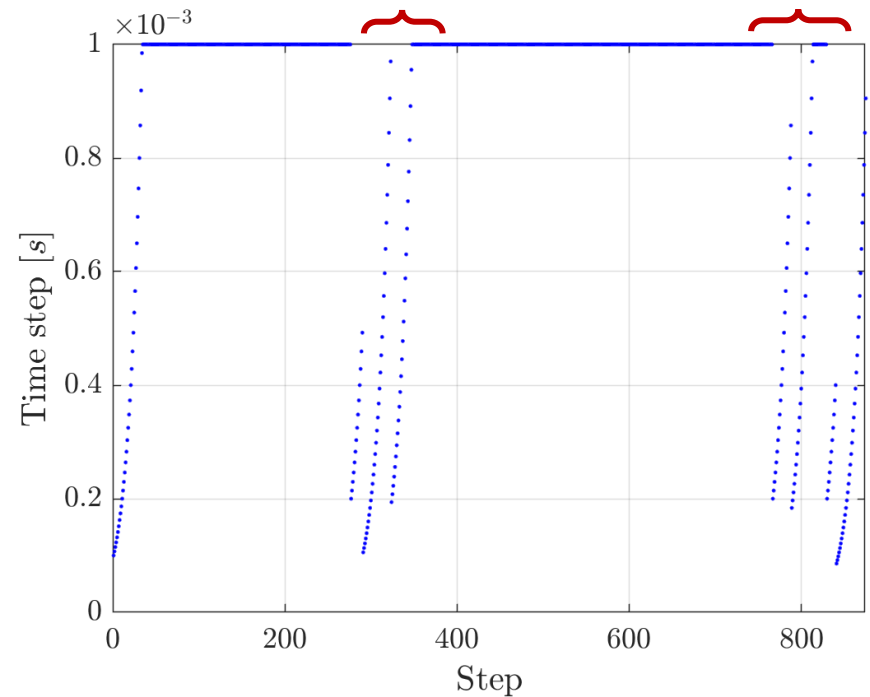
(A)

(B)

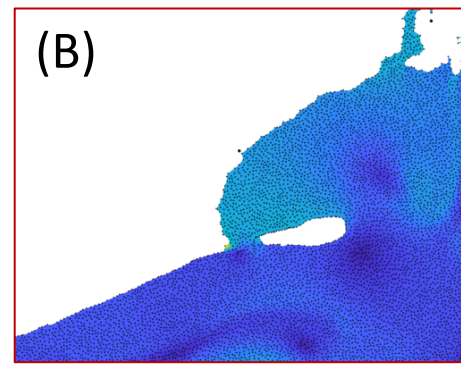
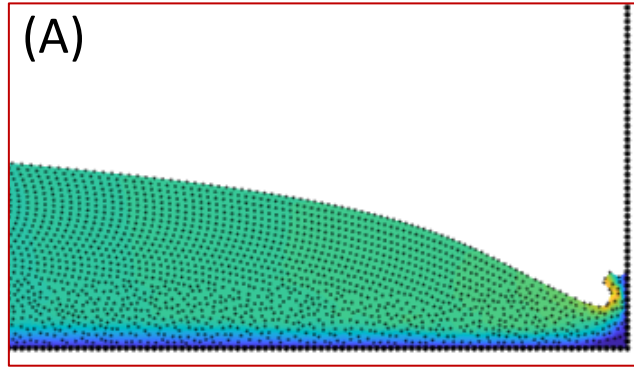


(A)

(B)



Study on the explicit time integration used in PFEM-2



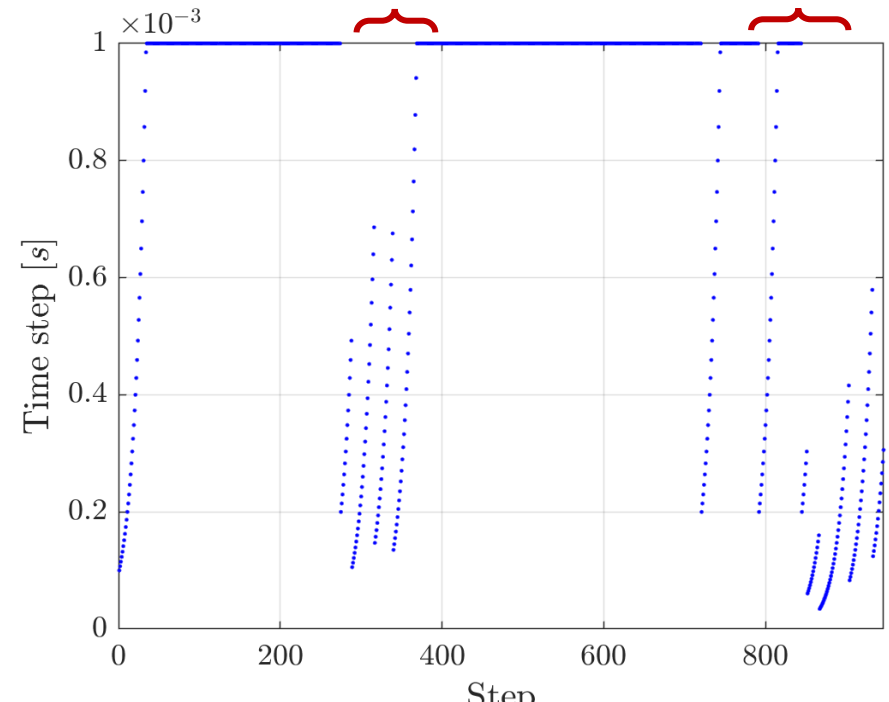
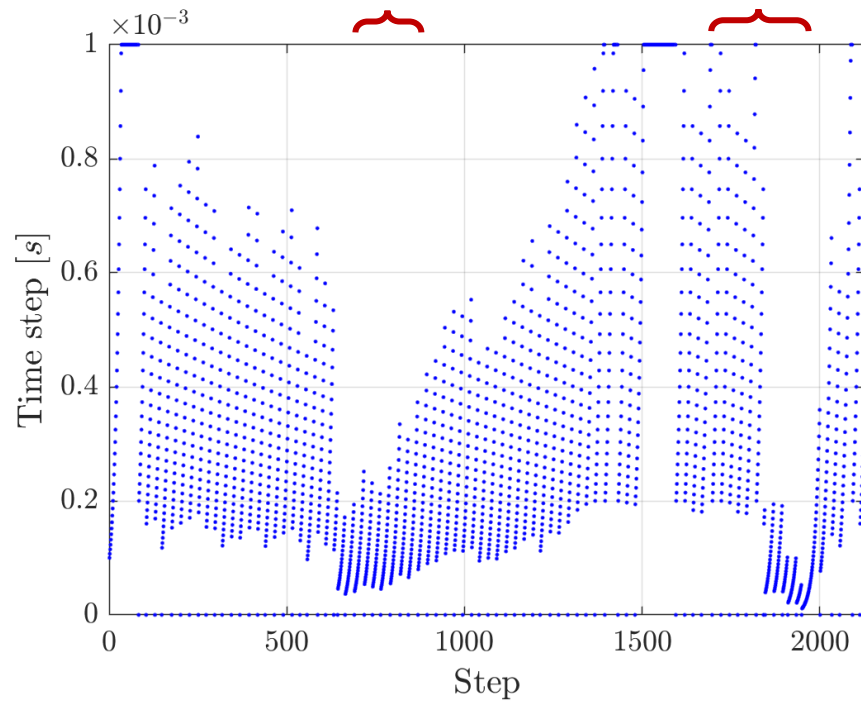
Reference

($h_{\text{char}} = 0.0009125$)

+ Remeshing (N-L loop)
+ XIVS integration

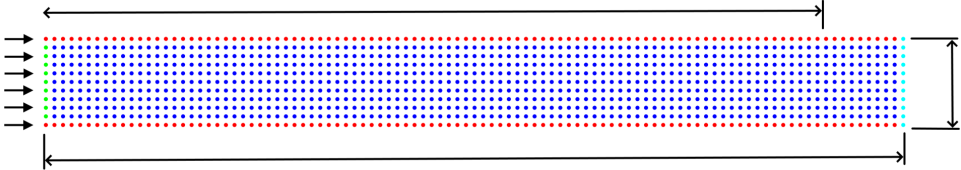
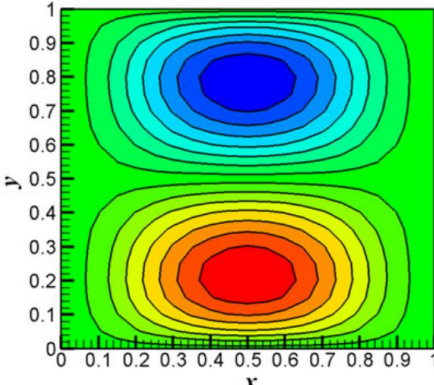
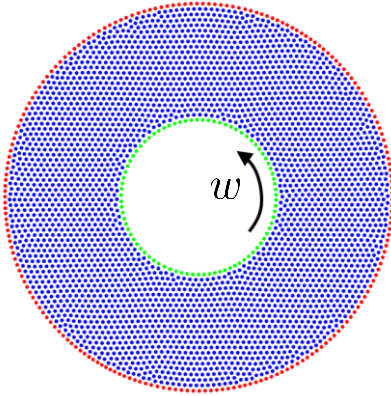
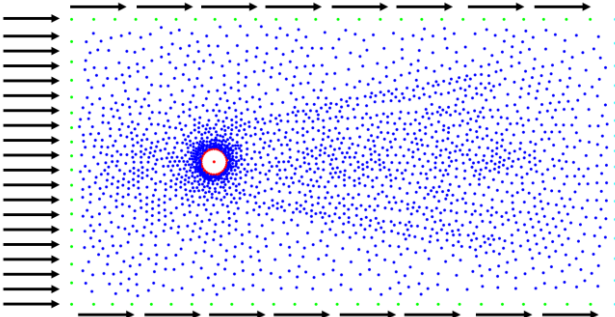
(A)

(B)



To do ...

- Compare

<div>Formulation</div> <div>Integration</div>	Velocity-Pressure	Position-Pressure
Backward-Euler	<div data-bbox="1091 382 1304 435">-- Using --</div> 	
α -Method		
+ XIVS (or Runge-Kutta)		

Oden & Jacquotte (1984)

To do ...

- Compare
- Similar study for the Fractional Step
- C++ implementation (PFEM3D)
- Include thermal simulation (as Marti & Ryzhakov)*

* Marti, J., & Ryzhakov, P. (2020). An explicit/implicit Runge-Kutta-based PFEM model for the simulation of thermally coupled incompressible flows. *Computational Particle Mechanics*, 7(1), 57-69.